

Related RSNs:
MDR: 1501736
Filing 1 ISP PDR: 1535408

1st Review - Please
contact Rifka Wine with
questions.
RWine@bhinc.com

PLEASE DO NOT RESUBMIT UNTIL COMMENTS
FROM OUTSIDE AGENCIES, AS LISTED BELOW,
HAVE BEEN RECEIVED.

Advisory note: PDR approval is
required prior to civil plan
approval.

MAINTENANCE ELIGIBILITY PROGRAM (MEP)

MHFD Referral Review Comments

For Internal MHFD Use Only.

MEP ID: 106325

Submittal ID: 10006190

MEP Phase: Referral

Date: April 30, 2021

To: Rifka Wine

Via Aurora Website

RE: MHFD Referral Review Comments

Project Name: Buckley Yard F2 (RSN 1535413)

Drainageway: East Toll Gate Creek

This letter is in response to the request for our comments concerning the referenced project. We have reviewed this proposal only as it relates to maintenance eligibility of major drainage features, in this case:

- Spillway and pipe outfalls from full spectrum detention ponds

We have the following comments to offer:

- 1) This site is within the 10,000' critical zone of Buckley Air Force Base. As such, the 100-yr flow of any ponds must drain within 40 hours. Please ensure the ponds meets this requirement.
- 2) The outflow for Pond A is much higher than the historic condition, increasing from approximately 26 cfs to 48 cfs. Can the existing culvert underneath E Alameda Dr accommodate these flows? Is there adequate protection downstream of this culvert in the existing condition?
- 3) Please evaluate the condition of the outfall paths from the proposed detention ponds. What protection will be provided for the spillway, if needed?

We appreciate the opportunity to review this proposal. Please feel free to contact me with any questions or concerns.

Sincerely,

Mark Schutte, P.E., CFM
Project Engineer, Sand Creek
Mile High Flood District

rt
g No. 2

JR Response:

1. Addressed.
2. Noted. This will be analyzed at time of final design. Pipe may need to be removed, upsized, and reworked downstream to accommodate.
3. Riprap will be provided for the spillway if needed.

	is Date
	Date
Water Department	Date

is an existing 18" RCP & 24" RCP storm sewer in the Northwest corner of E. Alameda Parkway and Alameda Drive at design point OS1. The 18" RCP conveys runoff from E. Alameda Parkway delineated as basin OS1 with a tributary area of 0.45 acres as shown on the historic and proposed conditions Map. The 24" RCP conveys stormwater runoff from areas south of Alameda Parkway including South Richfield St. and the detention pond from the TRW/Shea Center. The detention pond from the TRW site releases 3.75 cfs with a tributary area of 4.57 ac, per the approved Shea Center drainage report EDN: 201156. The 100-year runoff to the existing inlets along Richfield Street is 22.2 cfs per the Master Drainage Study for the Tollgate Village Filing No. 12 (COA# C8-2-1094). The culmination of the above discussed flows is designated as Design Point OS1 on the historic and proposed conditions map. The accumulation of the above offsite areas (5.02 acres) were used to size the water quality volume for Pond A. The existing 24" RCP that outfalls onto Buckley Yard was estimated to convey about 25.95 cfs from the total runoff, with a total pipe capacity of about 42 cfs. This flow is routed from design point OS1 north to Pond A via proposed storm pipe. The second offsite runoff location is an existing 24" RCP storm sewer on the Northwest corner of S. Quintero Way and E. Alameda Parkway as described as basin OS2 on the historic and proposed conditions map. This conveys runoff from E. Alameda Parkway. This flow is routed from design point OS1 north to Pond A via proposed storm pipe.

- b. The major drainage way adjacent to the property, North and East of the site, is East Tollgate Creek, which the site is tributary. East Tollgate Creek has a drainage area of about 9 square miles with a 100-year peak discharge of 8,100 cfs at Aurora Signature Park. A slight amount of the northeast edge of the property is located within the 100-year floodplain, as defined by FIRM map number 08005C0183L revised September 4, 2020. There is a 2020 FHAD for East Toll Gate Creek.

2. Drainage Patterns Through Property

The existing grades are generally sloping down in a northerly direction. The site is split into two major basins, Basin A in the west side of the property west of East Alameda Drive, and Basin B on the east side of the site between East Alameda Drive and South Quintero Way. Runoff from each basin will be conveyed to onsite water quality and detention ponds before being released. No onsite basins are proposed to flow offsite.

Offsite runoff from East Alameda Parkway and the properties to the south of Alameda Parkway will be conveyed through the site to the proposed ponds. JR Response: Addressed. The ponds will provide water quality for offsite runoff, but not detention.

3. Outfalls Downstream from Property

The ultimate outfall location for the site is East Toll Creek located directly to the north of the site. Currently there are 4 outfall locations from the site to East Toll Creek. In the proposed condition there are three outfall locations, the existing culvert at the

Gate

intersection of East Alameda Drive and South Quintero Way is to be removed as it is not needed.

C. DESIGN CRITERIA

1. List References

Add Buckley Yard Master Drainage Report (RSN 1501736). MDR has not yet been approved. Please do not resubmit until the MDR is approved.

- a. This report has been prepared in accordance with *Tollgate Village Filing No.14*, which encompasses the site. This was prepared by ICON Engineering, Inc.

JR Response: Addressed.

- b. This report has been prepared in accordance with *Tollgate Village Filing No.14*, which encompasses the site. This was prepared by MSM Consultants, Inc. EDN: C4-2-414

- c. This report has been prepared in accordance with *Bristol Commercial Center Filing Subdivision No. 6* Final Drainage Report (COA# 2001-3088). This was prepared by Innovative Land Consultants, Inc. EDN: 970218

- d. This report has been prepared in accordance with *Shea Center Subdivision Filing No. 1* Final Drainage Report (COA# 201156) EDN: 201156

Add Adjacent subdivision drainage report for Buckley Yard FLG #01 (RSN 1535408)

JR Response: Addressed. This report has been prepared in accordance with the specifications of the MHFCD's *Urban Storm Drainage Criteria Manual* (USDCM), as well as the City of Aurora *Storm Drainage Design & Technical Criteria Manual* (Criteria Manual).

- f. A very small portion of the property is located within the 100-year floodplain, while the vast majority of the site is not, as defined by FIRM map number 08005C0183L revised September 4, 2020. A copy of the FIRM can be found in Appendix 1 of this report.

2. Hydrologic Criteria

- a. Rainfall intensities were determined by the equations set forth in the Criteria Manual. Rainfall intensities were determined from the charts contained within the MHFCD and the City of Aurora Storm Drainage Design & Technical Criteria Manual. A P_1 value of 0.98 was used for the 2-year event and 2.66 for the 100-year event for the City of Aurora equations. A P_1 value of 1.01 was used for the 2-year event and 2.72 for the 100-year event for the MHFD equation per Figures RA-1 – RA-6 shown in Appendix D.

JR Response: Addressed.

MHFD (typ.)

- b. The Rational Method was utilized to determine runoff values for the site. Composite percent impervious values were calculated for the proposed basins. Water quality for the project will be provided in five onsite ponds. Calculations by volume were performed using the empirical formula as

Where are these? Only two are shown on drainage plan.

JR Response: Addressed. This was a mistake, there are only two ponds for this site.

- c. The Rational Method was utilized to determine runoff values for the site. Composite percent impervious values were calculated for the proposed basins. Water quality for the project will be provided in both Pond A and Pond B. The Full Spectrum Detention Method and empirical formula were utilized to calculate proposed detention pond volumes. Calculations utilizing the drain times per the FAA method to determine pond volumes has been provided.
- d. The minor storm was analyzed as the 2-year event. The major storm was analyzed as the 100-year event.

a. The *City of Aurora Storm Drainage and Technical Criteria Manual* were referenced in the preparation of this report.

b. All inlets and pipes will be designed for the 100-year storm. All storm sewers will be private and will be maintained by the special districts.

c. Storm drain pipe will be provided with the Final Drainage Report. The water surface profiles can be found in Appendix C.

4. East Tollgate Creek is the major drainage way located to the North and East of the site.

Which one? EDN 208094? Add Buckley Yard Master Drainage Report (RSN 1501736). MDR has not yet been approved.

1. General Concept

- ished with the **previously approved** drainage
posed on-site grading will continue to route
condition.

Label this inlet as sump on the drainage plans. Show this emergency overflow path with an arrow on the drainage plan.

JR Response: Addressed.

Basin A2 ($Q_2=3.7$ cfs, $Q_{100}= 12.0$ cfs) is 2.86 acres and 49.2 percent impervious and is comprised of multi-unit attached residential lots, alleyway, and roadway. Runoff from this basin is collected in the center alleys and drains to design point 2, a **sump** inlet at the north edge of the basin. Collected runoff is piped north to Pond A. The emergency overflow path of the **sump** inlet fills up and exits into adjacent curb and gutter heading north.

Basin A3 ($Q_2=4.6$ cfs, $Q_{100}= 13.8$ cfs) is 3.50 acres and 51.4 percent impervious and is comprised of multi-unit attached residential lots, alleyway, and roadway. Olsson Engineering is designing this north-south road; therefore the specifics of the drainage have not yet been determined. Runoff from this basin is collected in the street curb and gutter & inlets, draining to design point 15, an on grade inlet at the eastern edge of the basin. Collected runoff is piped east to Pond A.

sump?

Basin A5 ($Q_2=0.6$ cfs, $Q_{100}= 1.8$ cfs) is 0.26 acres and 77.3 percent impervious and is comprised of roadway. Runoff from this basin is collected in the gutter and drains to design point 3, an **on grade** inlet at the northwestern corner of the basin. Collected runoff is piped north to Pond A. The emergency overflow path of the **sump** inlet fills up and exits into adjacent curb and gutter heading north.

JR Response: Addressed.

Basin A6 ($Q_2=0.7$ cfs, $Q_{100}= 2.0$ cfs) is 0.34 acres and 62.9 percent impervious and is comprised of roadway. Runoff from this basin is collected in the street curb and gutter and drains to design point 7, an on grade inlet at the northwestern corner of the basin. Collected runoff is piped north to Pond A.

Basin A7 ($Q_2=0.5$ cfs, $Q_{100}= 1.6$ cfs) is 0.22 acres and 76.0 percent impervious and is comprised of roadway. Runoff from this basin is collected in the street curb and gutter and drains to design point 6, an on grade inlet at the northeastern corner of the basin. Collected runoff is piped north to Pond A.

Basin A8 ($Q_2=1.7$ cfs, $Q_{100}= 5.7$ cfs) is 1.67 acres and 38.9 percent impervious and is comprised of multi-unit attached residential lots, alleyway, 5' concrete walks, an open space park area, and a portion of South Quintero Way. Runoff from this basin is collected in the center alleys and curb and gutter then drains to design point 8, an on grade inlet at the northwestern corner of the basin. Collected runoff is piped north to Pond A.

Basin A9 ($Q_2=1.4$ cfs, $Q_{100}= 7.5$ cfs) is 1.79 acres and 46.2 percent impervious and is comprised of multi-unit attached residential lots, alleyway, and a portion of South Quintero Way. Runoff from this basin is collected in the center alleys and drains to design point 4, an on grade inlet at the northeastern corner of the basin. Collected runoff is piped north to Pond A.

Basin A10 ($Q_2=2.1$ cfs, $Q_{100}= 6.9$ cfs) is 1.60 acres and 43.7 percent impervious and is comprised of multi-unit attached residential lots, alleyway, open space, 5' walks, and a portion of South Quintero Way. Runoff from this basin is collected in the street curb and gutter and drains to design point 11, a **sump** inlet at the northern

Label this inlet as sump on the drainage plans. Show this emergency overflow path with an arrow on the drainage plan.

JR Response: Addressed.

edge of the basin. Collected runoff is piped north to Pond A. The emergency overflow path of the sump inlet fills up and exits into adjacent curb and gutter heading north.

Basin A11 ($Q_2=0.2$ cfs, $Q_{100}= 0.6$ cfs) is 0.09 acres and 80.0 percent impervious and is comprised of roadway. Runoff from this basin is collected in the street curb and gutter and drains to design point 14, an on grade inlet at the northeastern corner of the basin. Collected runoff is piped north to Pond A.

Basin A12 ($Q_2=0.2$ cfs, $Q_{100}= 0.5$ cfs) is 0.07 acres and 76.1 percent impervious and is comprised of roadway. Runoff from this basin is collected in the street curb and gutter and drains to design point 13, an on grade inlet at the northeastern corner of the basin. Collected runoff is piped north to Pond A.

JR Response: Addressed.
Note - Basins A15 & A16 are now combined with Basins A11 & A12. The sump inlet is now at DP11 in Basin A10. An emergency overflow path and cross section have been provided.

Basin A13 ($Q_2=1.4$ cfs, $Q_{100}= 4.5$ cfs) is 0.81 acres and 61.0 percent impervious and is comprised of multi-unit attached residential lots, alleyway, and 5' walks, and a portion of South Quintero Way. Runoff from this basin is collected in the street curb and gutter and drains to design point 9, an on grade inlet at the northeastern corner of the basin. Collected runoff is piped north to Pond A.

Basin A14 ($Q_2=0.2$ cfs, $Q_{100}= 0.5$ cfs) is 0.08 acres and 63.1 percent impervious and is comprised of a portion of South Quintero Way. Runoff from this basin is collected in the street curb and gutter and drains to design point 5, an on grade inlet at the north corner of the basin. Collected runoff is piped north to Pond A.

Describe the emergency overflow path for this inlet in the text.

Basin A15 ($Q_2=0.6$ cfs, $Q_{100}= 1.7$ cfs) is 0.26 acres and 71.0 percent impervious and is comprised of a portion of South Quintero Way. Runoff from this basin is collected in the street curb and gutter and drains to design point 12, a sump inlet at the northwestern corner of the basin. Collected runoff is piped north to Pond A.

Basin A16 ($Q_2=0.3$ cfs, $Q_{100}= 0.7$ cfs) is 0.11 acres and 73.2 percent impervious and is comprised of a portion of South Quintero Way. Runoff from this basin is collected in the street curb and gutter and drains to design point 10, an on grade inlet at the northeastern corner of the basin. Collected runoff is piped north to Pond A.

Basin A17 ($Q_2=2.4$ cfs, $Q_{100}= 7.9$ cfs) is 1.87 acres and 54.0 percent impervious and is comprised of multi-unit attached residential lots, alleyway, and 5' walks. Runoff from this basin is collected in the center alleys and curb and gutter then drains to design point 16, sump inlet at the northeastern corner of the basin. Collected runoff is piped south to Pond A. The emergency overflow path of the sump inlet fills up and exits into adjacent curb and gutter heading north along East Alameda Drive.

Basin A18 ($Q_2=0.4$ cfs, $Q_{100}= 1.2$ cfs) is 0.18 acres and 69.6 percent impervious and is comprised of roadway. Runoff from this basin is collected in the street curb and gutter and drains to design point 18, an on grade inlet at the northwestern corner of the basin. Collected runoff is piped east to Pond A.

Label this inlet as sump on the drainage plans. Show this emergency overflow path with an arrow on the drainage plan.

Basin A19 ($Q_2=0.4$ cfs, $Q_{100}= 1.3$ cfs) is 0.20 acres and 67.4 percent impervious and gutter and drains to design point 19, an on grade inlet at the northwestern corner of the basin. Collected runoff is piped east to Pond A. **JR Response: Addressed.**

sump?

JR Response: Addressed.

Basin A20 ($Q_2=0.2$ cfs, $Q_{100}= 0.7$ cfs) is 0.13 acres and 56.2 percent impervious and is comprised of roadway. Runoff from this basin is collected in the street curb and gutter and drains to design point 17, an on grade inlet at the northeastern corner of the basin. Collected runoff is piped south to Pond A. The emergency overflow path of the sump inlet fills up and exits into adjacent curb heading north along East Alameda Drive.

Ponds shall be 100% D

Basin A21 ($Q_2=2.2$ cfs, $Q_{100}= 6.9$ cfs) is 2.85 acres and 14.9 percent impervious and is comprised of open space area, 5' walks, a commercial recreation area. Runoff from this basin sheet flows and drains to design point 21, an on grade inlet at the northwestern corner of the basin. From the pond, treated stormwater is conveyed via existing 24" RCP under East Alameda Drive to East Toll Gate Creek. The emergency overflow of Pond A would exit onto curb and gutter along East Alameda Drive. **JR Response: Addressed. Pond % impervious is now 100%**

Basin B1 ($Q_2=0.9$ cfs, $Q_{100}= 5.0$ cfs) is 1.21 acres and 45.2 percent impervious and is comprised of multi-unit attached residential lots, alleyway, open space, and roadway. Runoff from this basin is collected in the center alleys and drains to design point 21, an on grade inlet at the northwestern corner of the basin. Collected runoff is piped northwest to Pond B.

Basin B2 ($Q_2=0.9$ cfs, $Q_{100}= 2.4$ cfs) is 0.63 acres and 37.9 percent impervious and is comprised of multi-unit detached residential lots, some open space, and roadway. Runoff from this basin is collected in the street curb and gutter and drains to design point 22, an on grade inlet at the southwestern corner of the basin. Collected runoff is piped northwest to Pond B.

Basin B3 ($Q_2=0.8$ cfs, $Q_{100}= 2.7$ cfs) is 0.69 acres and 47.2 percent impervious and is comprised of multi-unit attached residential lots, alleyway, open space, and roadway. Runoff from this basin is collected in the center alleys and drains to design point 25, an on grade inlet at the northwestern corner of the basin. Collected runoff is piped northeast to Pond B.

Basin B4 ($Q_2=0.2$ cfs, $Q_{100}= 0.6$ cfs) is 0.09 acres and 72.5 percent impervious and is comprised of roadway and alleyway. Runoff from this basin is collected in the street curb and gutter and drains to design point 26, an on grade inlet at the xxx corner of the basin. Collected runoff is piped xxx to Pond B.

Basin B5 ($Q_2=0.9$ cfs, $Q_{100}= 13.8$ cfs) is 3.55 acres and 45.2 percent impervious and is comprised of multi-unit attached residential lots, alleyway, open space, and roadway. Runoff from this basin is collected in the center alleys and drains to design point 23, a sump inlet at the northern edge of the basin. Collected runoff is

pipel northwest to Pond B. The emergency overflow path of the sump inlet fills up and exits into adjacent curb and gutter heading north.

sump?

JR Response: Addressed.

Basin B6 ($Q_2=0.9$ cfs, $Q_{100}=1.4$ cfs) is 0.30 acres and 48.9 percent impervious and is comprised of multi-unit detached residential lots and roadway. Runoff from this basin is collected in the street curb and gutter and drains to design point 24, an on grade inlet at the southwest corner of the basin. Collected runoff is pipel northwest to Pond B. The emergency overflow path of the sump inlet fills up and exits into adjacent curb and gutter heading north.

Label this inlet as sump on the drainage plans. Show this emergency overflow path with an arrow on the drainage plan.

Basin B7 ($Q_2=0.9$ cfs, $Q_{100}=1.8$ cfs) is 0.29 acres and 66.6 percent impervious and is comprised of roadway. Runoff from this basin is collected in the street curb and gutter and drains to design point 35, an on grade inlet at the northwestern corner of the basin. Collected runoff is pipel north to Pond B.

Basin B8 ($Q_2=0.9$ cfs, $Q_{100}=3.7$ cfs) is 0.82 acres and 47.7 percent impervious and is comprised of multi-unit detached residential lots and roadway. Runoff from this basin is collected in the street curb and gutter and drains to design point 34, an on grade inlet at the northwestern corner of the basin. Collected runoff is pipel north to Pond B.

Basin B9 ($Q_2=0.9$ cfs, $Q_{100}=1.6$ cfs) is 0.36 acres and 60.0 percent impervious and is comprised of a multi-unit detached residential lot and roadway. Runoff from this basin is collected in the street curb and gutter and drains to design point 27, an on grade inlet at the northeastern corner of the basin. Collected runoff is pipel north to Pond B.

Basin B10 ($Q_2=0.3$ cfs, $Q_{100}=1.0$ cfs) is 0.19 acres and 56.2 percent impervious and is comprised of a multi-unit detached residential lot and roadway. Runoff from this basin is collected in the street curb and gutter and drains to design point 28, an on grade inlet at the northwestern corner of the basin. Collected runoff is pipel north to Pond B.

Basin B11 ($Q_2=0.8$ cfs, $Q_{100}=2.8$ cfs) is 0.57 acres and 50.7 percent impervious and is comprised of multi-unit detached residential lots and roadway. Runoff from this basin is collected in the street curb and gutter and drains to design point 29, an on grade inlet at the northwestern corner of the basin. Collected runoff is pipel northwest to Pond B.

Basin B12 ($Q_2=0.7$ cfs, $Q_{100}=2.5$ cfs) is 0.53 acres and 45.1 percent impervious and is comprised of multi-unit detached residential lots and roadway. Runoff from this basin is collected in the street curb and gutter and drains to design point 30, an on grade inlet at the northeastern corner of the basin. Collected runoff is pipel northwest to Pond B.

Basin B13 ($Q_2=1.2$ cfs, $Q_{100}=3.8$ cfs) is 1.83 acres and 15.7 percent impervious and is comprised of an open space park area, multi-unit detached residential lots, and 5' concrete walks. Runoff from this basin is sheet flows and drains to design

point 31, an on grade inlet at the northwest edge of the basin. Collected runoff is piped northwest to Pond B.

Label this inlet as sump on the drainage plans. Show this emergency overflow path with an arrow on the drainage plan.

Basin B14 ($Q_2=0.4$ cfs, $Q_{100}= 1.1$ cfs) is 0.20 acres and 62.6 percent impervious and is comprised of roadway. Runoff from this basin is collected in the street curb and gutter and drains to design point 32, a sump inlet at the northern edge of the basin. Collected runoff is piped west to Pond B. The emergency overflow path of the sump inlet fills up and exits into adjacent curb and gutter heading north along South Quintero Way.

JR Response: Addressed.

Basin B15 ($Q_2=1.1$ cfs, $Q_{100}= 4.1$ cfs) is 0.91 acres and 45.5 percent impervious and is comprised of multi-unit detached residential lots and roadway. Runoff from this basin is collected in the street curb and gutter and drains to design point 33, a sump inlet at the northeastern corner of the basin. Collected runoff is piped west to Pond B. The emergency overflow path of the sump inlet fills up and exits into adjacent curb and gutter heading north along South Quintero Way.

Basin B16 ($Q_2=1.8$ cfs, $Q_{100}= 6.7$ cfs) is 1.56 acres and 45.9 percent impervious and is comprised of multi-unit detached residential lots and roadway. Runoff from this basin is collected in the street curb and gutter and drains to design point 37, a sump inlet at the western edge of the basin. Collected runoff is piped north to Pond B. The emergency overflow path of the sump inlet fills up and exits into adjacent curb and gutter heading northwest.

sump?

Basin B17 ($Q_2=0.5$ cfs, $Q_{100}= 1.7$ cfs) is 0.26 acres and 62.6 percent impervious and is comprised of roadway. Runoff from this basin is collected in the street curb and gutter and drains to design point 36, an on grade inlet at the northern edge of the basin. Collected runoff is piped north to Pond B. The emergency overflow path of the sump inlet fills up and exits into adjacent curb and gutter heading northwest.

JR Response: Addressed.

Basin B18 ($Q_2=4.5$ cfs, $Q_{100}= 14.4$ cfs) is 2.81 acres and 63.8 percent impervious and is comprised of multi-unit attached residential lots. Runoff from this basin is collected in the center alleys and drains to design point 38, an on grade inlet at the northern edge of the basin. Collected runoff is piped northeast to Pond B.

Basin B19 ($Q_2=0.3$ cfs, $Q_{100}= 0.8$ cfs) is 0.13 acres and 72.1 percent impervious and is comprised of roadway. Runoff from this basin is collected from the street curb and gutter and drains to design point 39, an on grade inlet at the northwestern corner of the basin. Collected runoff is piped northeast to Pond B.

Basin B20 ($Q_2=0.3$ cfs, $Q_{100}= 0.9$ cfs) is 0.15 acres and 63.1 percent impervious and is comprised of roadway. Runoff from this basin is collected from the street curb and gutter and drains to design point 40, an on grade inlet at the northeastern corner of the basin. Collected runoff is piped northeast to Pond B.

Ponds shall be 100% D

Basin B21 ($Q_2=0.9$ cfs, $Q_{100}= 3.1$ cfs) is 1.66 acres and 5.0 percent impervious and is comprised of open space and Pond B. Runoff from this basin is collected from the street curb and gutter and drains to design point 41, Pond B at the northwestern corner of the basin. From

JR Response: Addressed. Pond % impervious is now 100%

E. CONCLUSIONS

1. Compliance with Standards

City of Aurora *Storm Drainage Design and Technical Criteria Manual*, *Roadway Design and Construction Manual*, and *Urban Storm Drainage Criteria Manual* standards have all been complied with. All runoff up to the 100 year event will be safely conveyed through the site by storm drainage infrastructure and released to the outfall points in East Toll Gate Creek.

2. Summary of Concept

- a. The proposed design has taken into account contributing 100 year flows from onsite and offsite basins. Proposed drainage patterns conform to both historic and previously approved patterns. Stormwater infrastructure will be designed to convey the 100 year storm event. Detention and water quality has been provided for via the on-site full spectrum facilities.
- b. The proposed development will provide necessary inlets and water quality/detention facilities and stormwater infrastructure to provide adequate on-site drainage and enhancement to stormwater quality.
- c. The proposed project site will not have any adverse effects on the adjacent upstream or downstream areas. The drainage design generally follows the historic patterns and existing conveyances have been utilized whenever possible. The net effect of this development will be an increase in imperviousness and an increase in runoff flow rates. Streets, gutters, inlets and other storm sewer appurtenances have been designed to mitigate this increase.

LIST OF REFERENCES

1. City of Aurora Storm Drainage Design and Technical Criteria Manual, September 2010.
2. City of Aurora Roadway Design & Construction Specifications, September 2010.
3. City of Aurora Urban Storm Drainage Criteria Manual, Volumes 1, 2, and 3 Revised August 2018, Volume 2 September 2017, and Volume 3 November 2010.
4. Shea Center Subdivision Filing No. 14 Final Drainage Report, approved October 24, 2001. EDN: 201156
5. Final Drainage Report for Bristol Commercial Center Filing Subdivision Filing No. 6 approved November 20, 2018. EDN 21820
6. Final Drainage Report Tollgate Village Filing No. 14 approved August 20, 2008. EDN: 208094

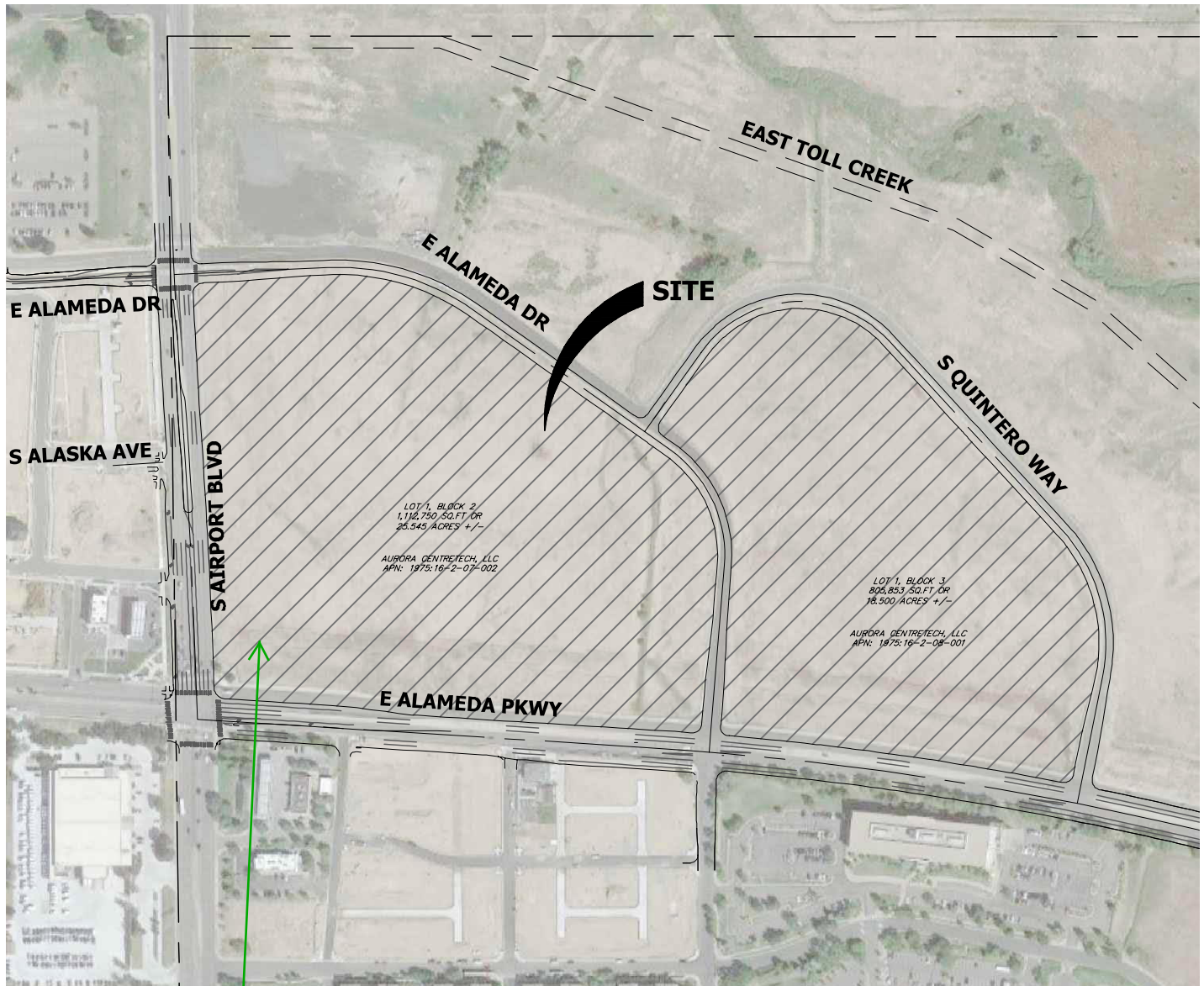
Add Buckley
Yard Master
Drainage Report
(RSN 1501736).
MDR has not yet
been approved.
Please do not
resubmit until the
MDR is
approved.

JR Response: Addressed.

Add Adjacent
subdivision
drainage
report for
Buckley Yard
FLG #01
(RSN
1535408)

JR Response: Addressed.

VICINITY MAP



Remove Filing 1
Area from
hatching.

JR Response: Addressed.

VICINITY MAP
BUCKLEY YARD
JOB NO. 16044.00
10/23/2020
SHEET 1 OF 1



J·R ENGINEERING
A Westrian Company

Centennial 303-740-9393 • Colorado Springs 719-593-2593
Fort Collins 970-491-9888 • www.jrengineering.com

EXISTING STANDARD FORM SF-2 TIME OF CONCENTRATION

Subdivision: Buckley Yard - Existing
Location: Aurora

Project Name: Aurora CentreTech
Project No.: 16044.00
Calculated By: CGV
Checked By: AJH
Date: 3/26/21

500 max

JR Response: Addressed.

SUB-BASIN						INITIAL/OVERLAND			TRAVEL TIME					t _c CHECK			FINAL
DATA						(T _i)			(T _t)					(URBANIZED BASINS)			
BASIN ID	D.A. (ac)	Hydrologic Soils Group	Impervious (%)	C ₂	C ₁₀₀	L (ft)	S _o (%)	t _i (min)	L _t (ft)	S _t (%)	K	VEL. (ft/s)	t _t (min)	COMP. t _c (min)	TOTAL LENGTH (ft)	Urbanized t _c (min)	
EX1	19.58	D	5%	0.18	0.22	533	1.1%	36.9	418	5.5%	10.0	2.3	3.0	39.9	951.0	15.3	15.3
EX2	18.67	D	5%	0.18	0.22	527	3.9%	24.3	91	3.3%	10.0	1.8	0.8	25.1	618.0	13.4	13.4
OS1	0.45	D	100%	0.87	0.93	133	1.1%	4.6	418	5.5%	20.0	4.7	1.5	6.1	551.0	13.1	6.1
OS2	0.40	D	100%	0.87	0.93	170	3.9%	3.4	117	3.3%	20.0	3.6	0.5	4.0	287.0	11.6	5.0

NOTES:

$$t_c = t_i + t_t \quad (5.2)$$

where t_c = time of concentration (minutes)
t_i = initial, inlet, or overland flow time (minutes)
t_t = travel time in the ditch, channel, gutter, storm sewer, etc. (minutes)

$$t_i = \frac{0.395(1.1 - C_s)\sqrt{L}}{\sqrt{S}} \quad (5.3)$$

where t_i = initial or overland flow time (minutes)
C_s = runoff coefficient for 5-year frequency
L = length of overland flow, (ft., 500 ft. max.)
S = average basin slope (ft/ft)

Use a minimum t_c value of 5 minutes for urbanized areas and a minimum t_c value of 10 minutes for areas that are not considered urban. Use minimum values even when calculations result in a lesser time of concentration.

$$I = \frac{28.5 P_1}{(10 + T_c)^{0.786}} \quad (5.5)$$

Where:

I = rainfall intensity (inches per hour)
P₁ = one-hour rainfall depth (inches) from Figures RA-1 through RA-6 in USDCM, Volume 1
T_c = time of concentration (minutes).

$$t_c = \frac{L'}{180} + 10 \quad (5.4)$$

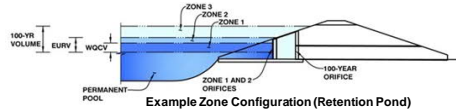
Where t_c = time of concentration (minutes)

L' = length of flow to first design point from the most remote point (feet)

Table 6-2. NRCS Conveyance factors, K

Type of Land Surface	Conveyance Factor, K
Heavy meadow	2.5
Tillage/field	5
Short pasture and lawns	7
Nearly bare ground	10
Grassed waterway	15
Paved areas and shallow paved swales	20

MHFD-Detention, Version 4.03 (May 2020)

Basin ID: Pond A

Example Zone Configuration (Retention Pond)

Selected BMP Type =	EDB	
Watershed Area =	19.70	acres
Watershed Length =	1.280	ft
Watershed Length to Centroid =	660	ft
Watershed Slope =	0.050	ft/ft
Watershed Imperviousness =	46.02%	percent
Percentage Hydrologic Soil Group A =	0.0%	percent
Percentage Hydrologic Soil Group B =	0.0%	percent
Percentage Hydrologic Soil Groups C/D =	100.0%	percent
Target WQCV Drain Time =	24.0	hours
Location for 1-hr Rainfall Depths =	User Input	

Drain Time Too Short

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

Water Quality Capture Volume (WQCV) =	0.321	acre-feet
Excess Urban Runoff Volume (EURV) =	0.852	acre-feet
2-yr Runoff Volume ($P1 = 1.01$ in.) =	0.740	acre-feet
5-yr Runoff Volume ($P1 = 1.41$ in.) =	1.308	acre-feet
10-yr Runoff Volume ($P1 = 1.66$ in.) =	1.698	acre-feet
25-yr Runoff Volume ($P1 = 2.02$ in.) =	2.345	acre-feet
50-yr Runoff Volume ($P1 = 2.36$ in.) =	2.910	acre-feet
100-yr Runoff Volume ($P1 = 2.72$ in.) =	3.574	acre-feet
500-yr Runoff Volume ($P1 = 3.14$ in.) =	4.280	acre-feet
Approximate 2-yr Detention Volume =	0.635	acre-feet
Approximate 5-yr Detention Volume =	1.067	acre-feet
Approximate 10-yr Detention Volume =	1.228	acre-feet
Approximate 25-yr Detention Volume =	1.428	acre-feet
Approximate 50-yr Detention Volume =	1.534	acre-feet
Approximate 100-yr Detention Volume =	1.818	acre-feet

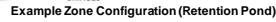
Zone 1 Volume (WCV_1)	=	0.321	acre-feet
Zone 2 Volume ($EURV - Zone 1$)	=	0.531	acre-feet
Zone 3 Volume (100-year - Zones 1 & 2)	=	0.966	acre-feet
Total Detention Basin Volume	=	1.818	acre-feet
Initial Surge Volume (ISV)	=	user	ft ³
Initial Surge Depth (ISD)	=	user	ft
Total Available Detention Depth (H_{TAD})	=	user	ft
Depth of Trickle Channel (H_{TC})	=	user	ft
Slope of Trickle Channel (Scr)	=	user	ft/ft
Slopes of Main Basin Sides (S_{Main})	=	user	H:V
Basin Length-to-Width Ratio ($R_{L/W}$)	=	user	
Initial Surge Area (A_{ISV})	=	user	ft ²
Surcharge Volume Length (LSV)	=	user	ft
Surcharge Volume Width (WSV)	=	user	ft
Depth of Basin Floor ($H_{f,100yr}$)	=	user	ft
Length of Basin Floor ($L_{f,100yr}$)	=	user	ft
Width of Basin Floor ($W_{f,100yr}$)	=	user	ft
Area of Basin Floor ($A_{f,100yr}$)	=	user	ft ²
Volume of Basin Floor ($V_{f,100yr}$)	=	user	ft ³
Depth of Main Basin (H_{Main})	=	user	ft
Length of Main Basin (L_{Main})	=	user	ft
Width of Main Basin (W_{Main})	=	user	ft
Area of Main Basin (A_{Main})	=	user	ft ²
Volume of Main Basin (V_{Main})	=	user	ft ³
Calculated Total Basin Volume (V_{Total})	=	user	acre-feet

Optional User Overrides

	acre-feet
	acre-feet
1.01	inches
1.41	inches
1.66	inches
2.02	inches
2.36	inches
2.72	inches
	inches

[illegible]

MHFD-Detention, Version 4.03 (May 2020)

Basin ID: Pond B

Drain Time Too Short

Optional User Overrides

	acre-feet
	acre-feet
1.01	inches
1.41	inches
1.66	inches
2.02	inches
2.36	inches
2.72	inches
	inches

Initial Surcharge Area (A_{SV})	=	user	ft ²
Surcharge Volume Length (L_{SV})	=	user	ft
Surcharge Volume Width (W_{SV})	=	user	ft
Depth of Basin Floor (H_{LLOOR})	=	user	ft
Length of Basin Floor (L_{LOOR})	=	user	ft
Width of Basin Floor (W_{LOOR})	=	user	ft
Area of Basin Floor (A_{LOOR})	=	user	ft ²
Volume of Basin Floor (V_{LOOR})	=	user	ft ³
Depth of Main Basin (H_{MAIN})	=	user	ft
Length of Main Basin (L_{MAIN})	=	user	ft
Width of Main Basin (W_{MAIN})	=	user	ft
Area of Main Basin (A_{MAIN})	=	user	ft ²
Volume of Main Basin (V_{MAIN})	=	user	ft ³
Calculated Total Basin Volume (V_{TBL})	=	USER	acre-feet

Do not include sizing of orifices or restrictor plates in PDR.

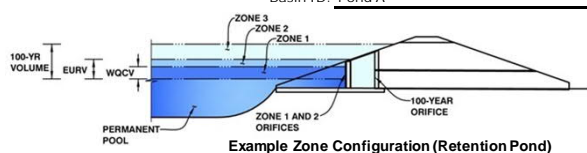
JR Response: Sheet included for emergency spillway calcs and elevation.

RETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.03 (May 2020)

Project: Aurora CentreTech

Basin ID: Pond A



Example Zone Configuration (Retention Pond)

	Estimated Stage (ft)	Estimated Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	1.98	0.321	Orifice Plate
Zone 2 (EURV)	3.07	0.531	Orifice Plate
Zone 3 (100-year)	4.63	0.966	Weir&Pipe (Restrict)
Total (all zones)		1.818	

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth =	N/A	ft (distance below the filtration media surface)
Underdrain Orifice Diameter =	N/A	inches

Calculated Parameters for Underdrain	
Underdrain Orifice Area =	N/A ft ²
Underdrain Orifice Centroid =	N/A feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice =	0.00	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Orifice Plate =	3.36	ft (relative to basin bottom at Stage = 0 ft)
Orifice Plate: Orifice Vertical Spacing =	13.40	inches
Orifice Plate: Orifice Area per Row =	3.16	sq. inches (diameter = 2 inches)

Calculated Parameters for Plate	
WQ Orifice Area per Row =	2.194E-02 ft ²
Elliptical Half-Width =	N/A feet
Elliptical Slot Centroid =	N/A feet
Elliptical Slot Area =	N/A ft ²

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	1.12	2.24					
Orifice Area (sq. inches)	3.16	3.16	3.16					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Not Selected	Not Selected	
Invert of Vertical Orifice =	N/A	N/A	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	N/A	N/A	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Diameter =	N/A	N/A	inches

Calculated Parameters for Vertical Orifice	
Vertical Orifice Area =	N/A ft ²
Vertical Orifice Centroid =	N/A feet

User Input: Overflow Weir (Dropbox with Flat or Sloped Gate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe))

	Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, H _o =	3.36	N/A	ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length =	5.00	N/A	feet
Overflow Weir Gate Slope =	4.00	N/A	H:V
Horiz. Length of Weir Sides =	4.00	N/A	feet
Overflow Gate Open Area % =	80%	N/A	%, gate open area/total area
Debris Clogging % =	50%	N/A	%

Calculated Parameters for Overflow Weir	
Height of Gate Upper Edge, H _u =	4.36 feet
Overflow Weir Slope Length =	4.12 feet
Gate Open Area / 100-yr Orifice Area =	6.64
Overflow Gate Open Area w/o Debris =	16.49 ft ²
Overflow Gate Open Area w/ Debris =	8.25 ft ²

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	2.50	N/A	ft (distance below basin bottom at Stage = 0 ft)
Outlet Pipe Diameter =	24.00	N/A	inches
Restrictor Plate Height Above Pipe Invert =	17.70		inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate	
Outlet Orifice Area =	2.48 ft ²
Outlet Orifice Centroid =	0.82 feet
Half-Central Angle of Restrictor Plate on Pipe =	2.07 radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage =	4.90	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	21.00	feet
Spillway End Slopes =	4.00	H:V
Freeboard above Max Water Surface =	1.00	feet

Calculated Parameters for Spillway	
Spillway Design Flow Depth =	0.92 feet
Stage at Top of Freeboard =	6.82 feet
Basin Area at Top of Freeboard =	0.76 acres
Basin Volume at Top of Freeboard =	2.80 acre-ft

Routed Hydrograph Results

The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).

	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period	N/A	N/A	1.01	1.41	1.66	2.02	2.36	2.72	3.14
One-Hour Rainfall Depth (in)	N/A	N/A	1.01	1.41	1.66	2.02	2.36	2.72	3.14
CUHP Runoff Volume (acre-ft)	0.321	0.852	0.740	1.308	1.698	2.345	2.910	3.574	4.280
Inflow Hydrograph Volume (acre-ft)	N/A	N/A	0.740	1.308	1.698	2.345	2.910	3.574	4.280
CUHP Predevelopment Peak Q (cfs)	N/A	N/A	1.5	8.5	12.4	22.1	28.9	36.8	45.2
OPTIONAL Override Predevelopment Peak Q (cfs)	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre)	N/A	N/A	0.07	0.43	0.63	1.12	1.47	1.87	2.29
Peak Inflow Q (cfs)	N/A	N/A	12.8	24.2	30.1	42.5	52.2	64.4	76.5
Peak Outflow Q (cfs)	0.2	0.4	0.4	1.7	4.8	13.8	21.2	30.5	39.5
Ratio Peak Outflow to Predevelopment Q	N/A	N/A	N/A	0.2	0.4	0.6	0.7	0.8	0.9
Structure Controlling Flow	Plate	Plate	Plate	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Spillway
Max Velocity through Gate 1 (fps)	N/A	N/A	N/A	0.1	0.3	0.8	1.3	1.8	1.9
Max Velocity through Gate 2 (fps)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours)	24	41	38	48	47	45	43	41	40
Time to Drain 99% of Inflow Volume (hours)	25	43	41	51	51	50	50	49	48
Maximum Ponding Depth (ft)	1.98	3.07	2.75	3.59	3.85	4.28	4.53	4.83	5.15
Area at Maximum Ponding Depth (acres)	0.37	0.57	0.53	0.60	0.62	0.65	0.66	0.68	0.70
Maximum Volume Stored (acre-ft)	0.324	0.857	0.679	1.162	1.321	1.587	1.757	1.959	2.180

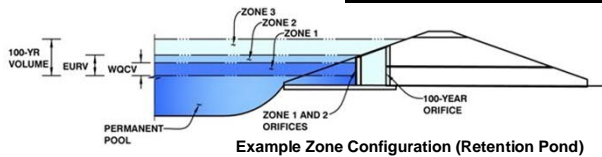
Do not include sizing of orifices or restrictor plates in PDR.

JR Response: Sheet included for emergency spillway calcs and elevation.

OUTLET STRUCTURE DESIGN

on, Version 4.03 (May 2020)

Project: Aurora CentreTech
Basin ID: Pond B



Example Zone Configuration (Retention Pond)

	Estimated Stage (ft)	Estimated Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	1.62	0.295	Orifice Plate
Zone 2 (EURV)	2.77	0.469	Orifice Plate
Zone 3 (100-year)	4.57	0.904	Weir&Pipe (Restrict)
Total (all zones)		1.668	

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = N/A ft (distance below the filtration media surface)
Underdrain Orifice Diameter = N/A inches

Calculated Parameters for Underdrain
Underdrain Orifice Area = N/A ft²
Underdrain Orifice Centroid = N/A feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice = 0.00 ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Orifice Plate = 3.36 ft (relative to basin bottom at Stage = 0 ft)
Orifice Plate: Orifice Vertical Spacing = 13.40 inches
Orifice Plate: Orifice Area per Row = 3.67 sq. inches (use rectangular openings)

Calculated Parameters for Plate
WQ Orifice Area per Row = 2.549E-02 ft²
Elliptical Half-Width = N/A feet
Elliptical Slot Centroid = N/A feet
Elliptical Slot Area = N/A ft²

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	1.12	2.24					
Orifice Area (sq. inches)	3.67	3.67	3.67					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Not Selected	Not Selected
Invert of Vertical Orifice =	N/A	N/A
Depth at top of Zone using Vertical Orifice =	N/A	N/A
Vertical Orifice Diameter =	N/A	N/A

ft (relative to basin bottom at Stage = 0 ft)
ft (relative to basin bottom at Stage = 0 ft)
inches

Calculated Parameters for Vertical Orifice
Vertical Orifice Area = N/A ft²
Vertical Orifice Centroid = N/A feet

User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe)

	Zone 3 Weir	Not Selected
Overflow Weir Front Edge Height, H _o =	2.78	N/A
Overflow Weir Front Edge Length =	4.00	N/A
Overflow Weir Grate Slope =	4.00	N/A
Horiz. Length of Weir Sides =	4.00	N/A
Overflow Grate Open Area % =	80%	N/A
Debris Clogging % =	50%	N/A

ft (relative to basin bottom at Stage = 0 ft)
feet
H:V
feet
%, grate open area/total area
%

Calculated Parameters for Overflow Weir
Height of Grate Upper Edge, H_u = 3.78 feet
Overflow Weir Slope Length = 4.12 feet
Grate Open Area / 100-yr Orifice Area = 6.47
Overflow Grate Open Area w/o Debris = 13.19 ft²
Overflow Grate Open Area w/ Debris = 6.60 ft²

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 3 Restrictor	Not Selected
Depth to Invert of Outlet Pipe =	2.50	N/A
Outlet Pipe Diameter =	30.00	N/A
Restrictor Plate Height Above Pipe Invert =	13.00	

ft (distance below basin bottom at Stage = 0 ft)
inches
Inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate
Outlet Orifice Area = 2.04 ft²
Outlet Orifice Centroid = 0.63 feet
Half-Central Angle of Restrictor Plate on Pipe = 1.44 radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage =	5.50	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	18.00	feet
Spillway End Slopes =	4.00	H:V
Freeboard above Max Water Surface =	1.00	feet

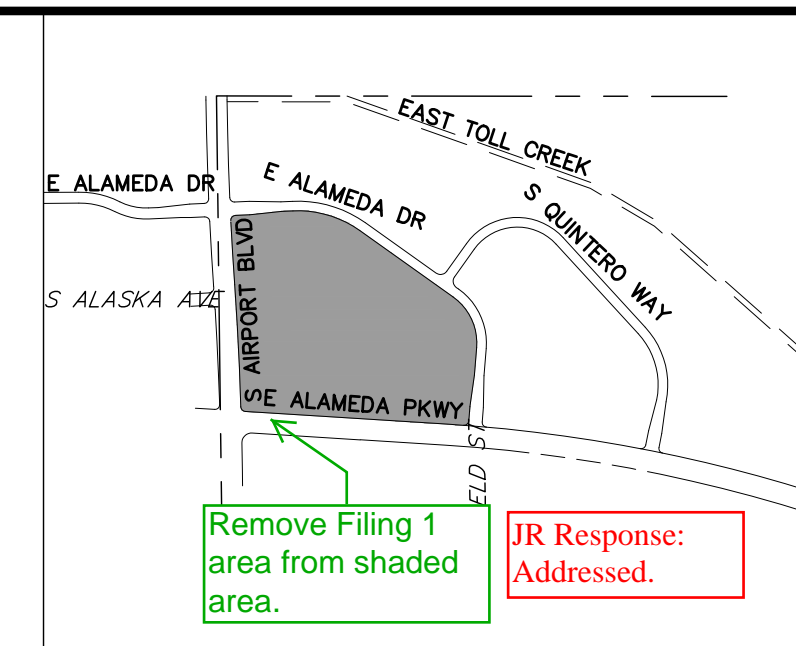
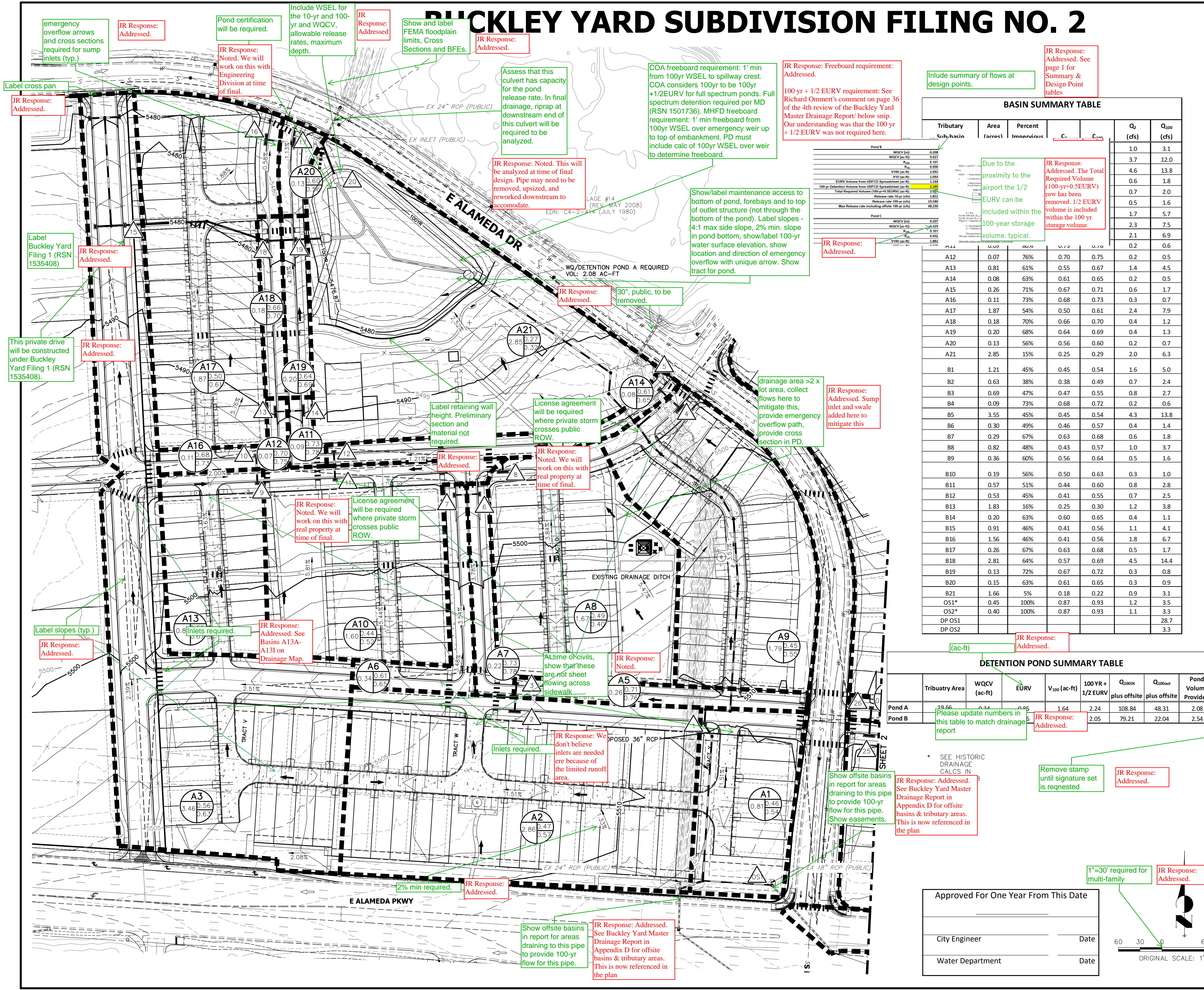
Calculated Parameters for Spillway
Spillway Design Flow Depth = 0.90 feet
Stage at Top of Freeboard = 7.40 feet
Basin Area at Top of Freeboard = 0.73 acres
Basin Volume at Top of Freeboard = 3.23 acre-ft

Routed Hydrograph Results

The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).

	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =	N/A	N/A	1.01	1.41	1.66	2.02	2.36	2.72	3.14
One-Hour Rainfall Depth (in) =	0.295	0.764	0.677	1.219	1.594	2.221	2.766	3.411	4.093
CUHP Runoff Volume (acre-ft) =	N/A	N/A	0.677	1.219	1.594	2.221	2.766	3.411	4.093
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	1.2	6.9	10.2	18.2	23.9	30.8	37.8
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A							
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.06	0.37	0.54	0.97	1.27	1.64	2.02
Peak Inflow Q (cfs) =	N/A	N/A	10.1	19.6	24.7	35.3	43.7	53.7	64.1
Peak Outflow Q (cfs) =	0.2	0.4	0.4	3.3	7.2	16.1	23.3	25.1	26.3
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.5	0.7	0.9	1.0	0.8	0.7
Structure Controlling Flow =	Plate	Plate	Plate	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Outlet Plate 1
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	0.2	0.5	1.2	1.7	1.8	1.9
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	24	39	38	42	41	39	37	35	33
Time to Drain 99% of Inflow Volume (hours) =	26	42	41	46	45	44	44	43	42
Maximum Ponding Depth (ft) =	1.62	2.77	2.43	3.20	3.46	3.85	4.09	4.64	5.31
Area at Maximum Ponding Depth (acres) =	0.38	0.45	0.42	0.47	0.49	0.51	0.53	0.56	0.61
Maximum Volume Stored (acre-ft) =	0.295	0.768	0.616	0.965	1.090	1.285	1.410	1.710	2.103

BUCKLEY YARD SUBDIVISION FILING NO. 2



LEGEND:

- PROPOSED STORM SEWER
- PROPOSED MAJOR CONTOUR
- PROPOSED MINOR CONTOUR
- EXISTING MAJOR CONTOUR
- EXISTING MINOR CONTOUR
- DRAINAGE BASIN
- DESIGN POINT
- HIGH POINT
- LOW POINT
- DRAINAGE ARROW
- EXISTING DRAINAGE ARROW
- POND EMERGENCY OUTFLOW
- PROPOSED DRAINAGE SWALE
- 100 YR FLOODPLAIN
- 500 YR FLOODPLAIN
- BASE FLOOD ELEVATION
- FEMA FLOODWAY
- EXISTING
- PROPOSED

BENCHMARK

ELEVATIONS ARE BASED OFF OF CITY OF AURORA CONTROL BENCHMARK NO. 0456616NW002 A 3" DIAM. BRASS CAP ON THE EAST SIDE OF A CURB OPENING INLET STRUCTURE BEING AT THE EAST PCR AT THE S.E. CORNER OF ALAMEDA PARKWAY AND S. BUCKLEY RD. SAID CAP BEING 3.0 FT. S. OF THE FLOWLINE. LOOPED TO AKA 11-053 BENCHMARK #0456616NW002 AURORA DATUM = 5503.43. NAVD 1988

NOTES:

- FEMA FLOODPLAIN INFORMATION OBTAINED FROM FIRM MAP NUMBER 08005C0183L EFFECTIVE 9/4/2020.
- ALL STORM INFRASTRUCTURE WILL BE PRIVATE AND WILL BE MAINTAINED BY THE SPECIAL DISTRICTS.
- ALL STORM INFRASTRUCTURE WILL BE PRIVATE AND SIZED FOR THE 100YR EVENT.

ENGINEER'S STATEMENT

THIS REPRODUCIBLE SEPIA IS A FACSIMILE OF A SIGNED AND SEALED PRINT TRANSMITTED TO THE CITY OF AURORA, ENGINEERING DEPARTMENT.

PREPARED UNDER MY SUPERVISION

(KURTIS WILLIAMS), P.E.
COLORADO P.E. 34270
FOR AND ON BEHALF OF JR ENGINEERING, LLC.

CITY OF AURORA PLAN REVIEW IS ONLY FOR GENERAL CONFORMANCE WITH CITY OF AURORA DESIGN CRITERIA AND THE CITY CODE. THE CITY IS NOT RESPONSIBLE FOR THE ACCURACY AND ADEQUACY OF THE DESIGN, OF DIMENSIONS AND ELEVATIONS WHICH SHALL BE CONFIRMED AND CORRELATED AT THE JOB SITE. THE CITY OF AURORA, THROUGH THE APPROVAL OF THIS DOCUMENT, ASSUMES NO RESPONSIBILITY FOR THE COMPLETENESS AND/ OR ACCURACY OF THIS DOCUMENT.

BASIN SUMMARY TABLE

Tributary Sub-basin	Area (acres)	Percent Impervious	C _s	C ₁₀₀	Q _s (cfs)	Q ₁₀₀ (cfs)
Pond B	0.208	0.427	0.107	0.056	1.0	3.1
WQCV (ac-ft)	0.427	0.107	0.056	0.026	3.7	12.0
V ₁₀₀ (ac-ft)	2.092	1.093	1.144	2.295	4.6	13.8
100-yr Detention Volume from UDFCD Spreadsheet (ac-ft)	2.295	1.144	2.295	1.851	0.6	1.8
Total Required Volume (100-yr + 50-yr) (ac-ft)	1.851	1.144	1.851	1.851	0.7	2.0
Release rate 10-yr (cfs)	13.580	1.851	1.851	1.851	0.5	1.6
Max Release rate including offsite 100-yr (cfs)	48.230	1.851	1.851	1.851	1.7	5.7
Pond C	0.207	0.427	0.107	0.056	2.3	7.5
WQCV (ac-ft)	0.427	0.107	0.056	0.026	2.1	6.9
V ₁₀₀ (ac-ft)	2.092	1.093	1.144	2.295	0.2	0.6
100-yr Detention Volume from UDFCD Spreadsheet (ac-ft)	2.295	1.144	2.295	1.851	0.2	0.5
Total Required Volume (100-yr + 50-yr) (ac-ft)	1.851	1.144	1.851	1.851	1.4	4.5
Release rate 10-yr (cfs)	13.580	1.851	1.851	1.851	0.2	0.5
Max Release rate including offsite 100-yr (cfs)	48.230	1.851	1.851	1.851	0.6	1.7
Pond A	0.07	76%	0.70	0.75	0.2	0.5
A12	0.07	76%	0.70	0.75	0.2	0.5
A13	0.81	61%	0.55	0.67	1.4	4.5
A14	0.08	63%	0.61	0.65	0.2	0.5
A15	0.26	71%	0.67	0.71	0.6	1.7
A16	0.11	73%	0.68	0.73	0.3	0.7
A17	1.87	54%	0.50	0.61	2.4	7.9
A18	0.18	70%	0.66	0.70	0.4	1.2
A19	0.20	68%	0.64	0.69	0.4	1.3
A20	0.13	56%	0.56	0.60	0.2	0.7
A21	2.85	15%	0.25	0.29	2.0	6.3
B1	1.21	45%	0.45	0.54	1.6	5.0
B2	0.63	38%	0.38	0.49	0.7	2.4
B3	0.69	47%	0.47	0.55	0.8	2.7
B4	0.09	73%	0.68	0.72	0.2	0.6
B5	3.55	45%	0.45	0.54	4.3	13.8
B6	0.30	49%	0.46	0.57	0.4	1.4
B7	0.29	67%	0.63	0.68	0.6	1.8
B8	0.82	48%	0.43	0.57	1.0	3.7
B9	0.36	60%	0.56	0.64	0.5	1.6
B10	0.19	56%	0.50	0.63	0.3	1.0
B11	0.57	51%	0.44	0.60	0.8	2.8
B12	0.53	45%	0.41	0.55	0.7	2.5
B13	1.83	16%	0.25	0.30	1.2	3.8
B14	0.20	63%	0.60	0.65	0.4	1.1
B15	0.91	46%	0.41	0.56	1.1	4.1
B16	1.56	46%	0.41	0.56	1.8	6.7
B17	0.26	67%	0.63	0.68	0.5	1.7
B18	2.81	64%	0.57	0.69	4.5	14.4
B19	0.13	72%	0.67	0.72	0.3	0.8
B20	0.15	63%	0.61	0.65	0.3	0.9
B21	1.66	5%	0.18	0.22	0.9	3.1
OS1*	0.45	100%	0.87	0.93	1.2	3.5
OS2*	0.40	100%	0.87	0.93	1.1	3.3
DP OS1						28.7
DP OS2						3.3

DETENTION POND SUMMARY TABLE

Tributary Area	WQCV (ac-ft)	EURV	V ₁₀₀ (ac-ft)	100YR + 1/2 EURV	Q _{100in} plus offsite	Q _{100out} plus offsite	Pond Volume Provided
Pond A	19.66	0.24	1.64	2.24	108.84	48.31	2.08
Pond B	19.66	0.24	1.64	2.24	108.84	48.31	2.08

JR Response: Noted. The permit will be processed at the time of final design. Finished floor elevation will be a minimum of 2' above the BFE and lots will be a minimum of 1' above the BFE.

Label retaining wall height. Preliminary section and material not required. At time of civils, be advised to submit a structural report for these walls that takes account saturated soil conditions, potentially global stability analysis depending on spacing of walls and height of walls.

Advisory note: storm drain in alley, potential utility conflicts. How will manholes work in valley gutter, provide details at time of civils.

Floodplain Development Permit will be required. Show setbacks and FFEs for lots adjacent to floodplain. LFEs required to be 2 ft min above BFE. Lots required to be 1 ft min above BFE. Elevation certificates will be required at the time of civil plans for lots adjacent to pond.

24", label as public, assess that this culvert has capacity for the pond release rate. In final drainage, riprap at downstream end of this culvert will be required to be analyzed. Backflow preventer device may be required. Use Toll Gate 100-yr BFE as tailwater for pond outfall.

Pond certification will be required.

JR Response: Noted. We will work on this at time of final design.

Include 10-yr and 100-yr volumes (including WQCV), WSEL for the 10-yr and 100-yr and WQCV, allowable release rates, maximum depth.

Show and label FEMA floodplain limits, Cross Sections and BFEs.

COA freeboard requirement: 1' min from 100yr WSEL to spillway crest. COA considers 100yr to be 100yr +1/2EURV for full spectrum ponds. Full spectrum detention required per MD (RSN 1501736). MHFD freeboard requirement: 1' min freeboard from 100yr WSEL over emergency weir up to top of embankment. PD must include calc of 100yr WSEL over weir to determine freeboard.

JR Response: See page 1 response.

Label BFEs and FEMA XSECS

JR Response: Addressed.

Show/label maintenance access to bottom of pond, forebays, and to top of outlet structure (not through the bottom of the pond). Label slopes - 4:1 max side slope, 2% min. slope in pond bottom, show/label 100-yr water surface elevation, show location and direction of emergency overflow with unique arrow. Show tract for pond.

JR Response: Addressed.

Show flow direction arrows

JR Response: Addressed.

Show, dimension, and label ROW, existing and proposed easements (drainage, utility, fire land, etc.), and tract dimensions.

JR Response: Addressed.

emergency overflows required for sump inlets (provide cross section and flow arrow, show that it can overtop high point in street, place top of foundation above that)

JR Response: Addressed. See Appendix C sump inlet overflow cross sections.

Use higher of BFE and 100-yr pond elevation for tailwater for HGL analysis. Please include HGL analysis in this PDR far enough upstream to demonstrate that discharging into Toll Gate Creek is not going to flood any of the lots, due to the tailwater concerns from the Toll Gate Creek BFE.

JR Response: HGL analysis will be completed at the time of final design.

At time of civils, show that it is not sheet flowing across sidewalk.

JR Response: Noted.

Garage slabs must be 0.5' above 100-yr, finished floor 1' above 100-yr WSE in alley.

JR Response: Addressed. See Appendix C concrete Alley Hydraulics

Label slope

JR Response: Addressed.

must treat for offsite areas (I calculate 0.29 ac-ft)

JR Response: Addressed. WQCV calculated to be 0.276 ac-ft using 18.74 ac of Basin B & 0.4 ac of offsite area.

calculate 0.85 for Pond B

JR Response: Addressed. EURV is 0.781 ac-ft per Pond B MHFD spreadsheet.

Please update numbers in this table to match drainage report

JR Response: Addressed.

Remove stamp until signature set is requested

JR Response: Addressed.

This is only required on first sheet of drainage plan.

JR Response: Addressed.

1"=30' required for multi-family

JR Response: Addressed.

Approved For One Year From This Date	
City Engineer	Date
Water Department	Date



BASIN SUMMARY TABLE						
Tributary Sub-basin	Area (acres)	Percent Impervious	C ₂	C ₁₀₀	Q ₂ (cfs)	Q ₁₀₀ (cfs)
A1	0.81	46%	0.46	0.54	1.0	3.1
A2	2.86	49%	0.47	0.57	3.7	12.0
A3	3.46	59%	0.56	0.63	4.6	13.8
A5	0.26	78%	0.71	0.76	0.6	1.8
A6	0.34	63%	0.61	0.65	0.7	2.0
A7	0.22	76%	0.70	0.75	0.5	1.6
A8	1.67	39%	0.40	0.49	1.7	5.7
A9	1.79	46%	0.45	0.55	2.3	7.5
A10	1.60	44%	0.44	0.53	2.1	6.9
A11	0.09	80%	0.73	0.78	0.2	0.6
A12	0.07	76%	0.70	0.75	0.2	0.5
A13	0.81	61%	0.55	0.67	1.4	4.5
A14	0.08	63%	0.61	0.65	0.2	0.5
A15	0.26	71%	0.67	0.71	0.6	1.7
A16	0.11	73%	0.68	0.73	0.3	0.7
A17	1.87	54%	0.50	0.61	2.4	7.9
A18	0.18	70%	0.66	0.70	0.4	1.2
A19	0.20	68%	0.64	0.69	0.4	1.3
A20	0.13	56%	0.56	0.60	0.2	0.7
A21	2.85	15%	0.25	0.29	2.0	6.3
B1	1.21	45%	0.45	0.54	1.6	5.0
B2	0.63	38%	0.38	0.49	0.7	2.4
B3	0.69	47%	0.47	0.55	0.8	2.7
B4	0.09	73%	0.68	0.72	0.2	0.6
B5	3.55	45%	0.45	0.54	4.3	13.8
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DETENTION POND SUMMARY TABLE								
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Pond A	19.66	0.34	0.53	1.82	2.08	108.84	48.31	2.08
Pond B	18.74	0.04	0.47	1.67	1.90	79.21	22.04	2.54

LEGEND:

- PROPOSED STORM SEWER
- 5000 PROPOSED MAJOR CONTOUR
- PROPOSED MINOR CONTOUR
- 5000 EXISTING MAJOR CONTOUR
- EXISTING MINOR CONTOUR
- DRAINAGE BASIN
- A = BASIN DESIGNATION
- B = AREA IN ACRES
- C = 2-YR RUNOFF COEFFICIENT
- D = 100-YR RUNOFF COEFFICIENT
- DESIGN POINT
- HIGH POINT
- LOW POINT
- DRAINAGE ARROW
- EXISTING DRAINAGE ARROW
- POND EMERGENCY OUTFLOW
- PROPOSED DRAINAGE SWALE
- 100 YR FLOODPLAIN
- 500 YR FLOODPLAIN
- 54XX BASE FLOOD ELEVATION
- FEMA FLOODWAY
- EXISTING
- PROPOSED

BENCHMARK

ELEVATIONS ARE BASED OFF OF CITY OF AURORA CONTROL BENCHMARK NO. 04S6616NW002 A 3" DIAM. BRASS CAP ON THE EAST SIDE OF A CURB OPENING INLET STRUCTURE BEING AT THE EAST PCR AT THE S.E. CORNER OF ALAMEDA PARKWAY AND S. BUCKLEY RD. SAID CAP BEING 3.0 FT. S. OF THE FLOWLINE. LOOPED TO AKA 11-053 BENCHMARK #0456616NW002 AURORA DATUM = 5503.43. NAVD 1988

NOTES:

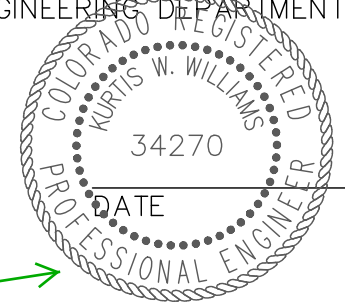
- FEMA FLOODPLAIN INFORMATION OBTAINED FROM FIRM MAP NUMBER 08005C0183L EFFECTIVE 9/4/2020.
- ALL STORM INFRASTRUCTURE WILL BE PRIVATE AND WILL BE MAINTAINED BY THE SPECIAL DISTRICTS.
- ALL STORM INFRASTRUCTURE WILL BE PRIVATE AND SIZED FOR THE 100YR EVENT.

ENGINEER'S STATEMENT

THIS REPRODUCIBLE SEPIA IS A FACSIMILE OF A SIGNED AND SEALED PRINT TRANSMITTED TO THE CITY OF AURORA, ENGINEERING DEPARTMENT.

PREPARED UNDER MY SUPERVISION

(KURTIS WILLIAMS), P.E.
COLORADO P.E. 34270
FOR AND ON BEHALF OF JR ENGINEERING, LLC.



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PROPOSED CONDITIONS MAP
BUCKLEY YARD
JOB NO. 16044.00
04/12/21
SHEET 2 OF 2



Centennial 303-740-9993 • Colorado Springs 719-593-2593
Fort Collins 970-491-9888 • www.jrengineering.com