

# Final Drainage Letter

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Eastern Hills South 4-65 17-18 3AH-3DH, 4AH-4DH Pad  
Aurora Condition Use Permit  
City of Aurora Case No. DA-2155-00

Prepared for:

ConocoPhillips Company  
34501 E. Quincy Ave., Bldg. 1  
Watkins, CO 80137  
303-268-3773  
Kathy Denzer

Prepared by:

Ascent Geomatics Solutions  
8620 Wolff Court  
Westminster, CO 80031  
303-928-7128  
Michael Welker

**Rev. 3 January 27, 2020**

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## **FACSIMILE**

This electronic plan is a facsimile of the signed and sealed PDF set.



DATE: 01/27/2020

Michael C. Welker

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Rev. 3 January 27, 2020

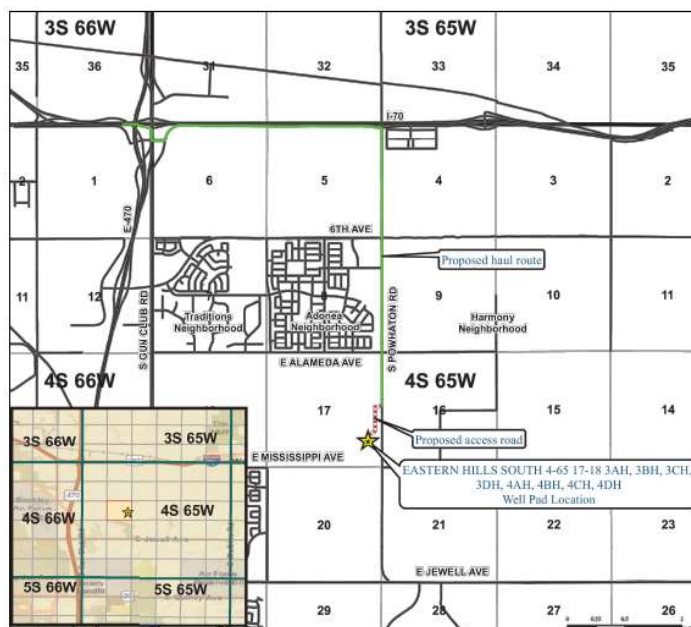


Craig Perl, P.E. Senior Engineer  
City of Aurora  
Public Works Department  
Engineering Control Division  
15151 E. Alameda Avenue  
Aurora, CO 80012

**RE: Eastern Hills South 4-65 17-18 3AH-3DH, 4AH-4DH Pad**  
**City of Aurora Oil and Gas Well Permit**  
**Final Drainage Letter**  
**City of Aurora Case No. DA-2155-00**

Dear Mr. Perl,

The Eastern Hills South 4-65 17-18 3AH-3DH, 4AH-4DH Pad (hereafter referred to as "Site") is located in Section 17, Township 4 South, Range 65 West of the 6<sup>th</sup> Principal Meridian, in the City of Aurora, Arapahoe County, Colorado. The pad is generally located approximately 2.8 miles south of I-70 and approximately 2.5 miles east of Highway E-470. More specifically the pad is located along South Powhatan Road approximately 6,500 feet north of East Jewell Avenue (County Road 18) and 8,000 feet south of East 3<sup>rd</sup> Avenue. The 3<sup>rd</sup> Avenue and Powhatan Road intersection serves as a secondary entrance to the Traditions residential development. The Site is also 1 mile northeast of the Murphy Creek residential development. A vicinity map is included as Figure 1 below.



The existing landscape and land use of the proposed Site is rangeland or grazing land and the Site is zoned Northeastern Plains Residential. The existing topography generally drains from southeast to northwest at an existing grade of the disturbed area is approximately 0.3 -1%, with the undisturbed upstream basin having slopes of approximately 1% to 11% slope. According to the USDA Web Soil Survey contains exclusively Nunn-Bresser-Ascalon complex, hydrologic Type B soils in the disturbed areas. The upstream basin contains a percentage of Truckton loamy sand, Type A hydrologic soils in the southeast corner of the basin. The web Soil Map and Descriptions are attached.

Proposed improvements include a 500 foot by 580 foot graded pad in support of drilling oil and gas wells. Also proposed is a 1,450-linear foot, 23-foot wide gravel access road, connecting to another site access approximately 1,300 feet north the Site. This access road connects another drill pad to the northwest to South Powhatan Road, which is immediately to the east of the pad.

Eight proposed wellheads are located 375 feet west of the east edge of the pad, spaced 25 feet apart with the northern-most well located 150 feet south of the north edge of the pad and the southern-most well located 174 feet north of the south edge of the pad.

The Site is located within the Coal Creek drainage basin. As indicated by the attached FEMA FIRMette, the proposed Site is within FIRM Panel Number 08005C0208L, panel 208 of 725, dated February 17, 2017. The pad is shown to be located within unshaded Flood Zone X, an area outside the 0.2% annual chance floodplain. The Site is not included within a Special Flood Hazard Area and therefore FEMA considers it an area of minimal flooding.

The design of the Site drainage, is based on the Urban Drainage and Flood Control District Urban Storm Drainage Criteria Manual (USCM) design guides and best practices, and the deviations from these best practices listed in the City of Aurora's *Rules and Regulations Regarding Stormwater Discharges Associated with Construction Activities and Storm Drainage and Technical Criteria*.

The onsite and offsite diversion ditches, and the sediment capture volumes were calculated using the rational method due to the relatively small sub basin sizes. These sub-basins are illustrated in the attached Drainage Basin Boundary Map. The proposed onsite and offsite diversion ditches, and culverts were sized for the 100 year 1 hour storm using Figure RA-6 from UDFCD Volume 1, see attached. The hydrologic calculations were used in the Urban Drainage Rational Workbook attached.

The Site gravel pad was assumed to be the 40 percent impervious for gravel roads, and the offsite drainage was assumed to be the 2% Historic Flow Analysis, Greenbelts, and Agricultural imperviousness listed in the Aurora Drainage and Technical Criteria Appendix Table 1. The

onsite and offsite ditches we divided into east and west by the high point on the southeast corner of the Site.

The onsite pad for the drilling phase is 7.82 acres with an overall surface disturbance of 11.45 acres. The disturbance area is comprised of the onsite basin, seeded topsoil stockpile, seeded excess stockpiles, Sediment Basin, and diversion swales. The production phase pad surface (4.42 acres) itself is not included in the tributary area used to size the sediment basin as agreed upon by the Aurora Water Department. Therefore, the sediment basin was sized for 7.03 acres (11.45ac.- 4.42ac.). The sediment basin is located near the northwest corner of the pad, includes 1' of freeboard, and will be used as a permanent BMP (to be maintained by the Site owner) to enhance the water quality of the runoff from the Site as long as there is activity on the Site. Due to vertical constraints the sediment basin is shallower than the preferred, standard basin but will have a larger footprint to meet storage requirements. The basin was sized according to COA Storm Drainage Design and Technical Criteria Manual Table 1 and UDFCD Table SB-1. An outlet structure has been designed with four orifice holes (2"H x 4"W) to drain the sediment basin in less than 72 hours. Please see the attached Drainage Basin Boundary Map, Sediment Basin Stage-Storage, and Stormwater Detention and Infiltration spreadsheets.

Four culverts are proposed for the Site. Culvert A is for Diversion Ditch 1 collecting the eastern flows under the proposed access road connection the pad within Onsite Basin 1. This culvert is designed as a 1.25'x7.5' open channel with cattle guard. Culvert B is designed to carry flow from Offsite Basin 2 under the proposed access road near its northern terminus. This culvert is designed as a 1'x7' open channel with cattle guard. Culvert C is located in the proposed access road approximately 310 feet north of the pad at the existing drainage swale. Culvert C is designed as a 24" RCP to handle offsite flows from Offsite Basin 3 under the raised access road. Finally, Culvert D is located in the proposed access road approximately 145 feet north of the pad at the existing drainage swale. Culvert D is designed as a 12" RCP to handle offsite flows from Offsite Basin 4 under the raised access road. Type M (12") riprap reinforcement will be placed at each of the culvert outlets. Culvert calculations are detailed in the UD Culvert workbooks attached.

The Rational Method was used to compute peak flows draining into the two onsite diversion ditches. The catchment area draining into Onsite Diversion Ditch 1 was found to be 12.04 acres with an imperviousness of 11% resulting in a 100-year flow rate of 17.72 cfs. Onsite Diversion Ditch 1 capable of conveying 18.68 cfs has been designed, with a 3:1 side slope, a minimum slope of 0.11%, a total depth of 1.25', and a bottom width of 7.5'. Flow in Diversion Ditch 1 will pass through Culvert A before reaching the sediment basin. The catchment area draining into Onsite Diversion Ditch 2 was found to be 4.13 acres with an imperviousness of 35% resulting in a 100-year flow rate of 11.70 cfs. Onsite Diversion Ditch 2 capable of conveying 15.76 cfs has been designed, with a 3:1 side slope, a minimum slope of 0.11%, a total depth of 1.25', and a



bottom width of 6'. Onsite Diversion Ditch 2 will be relocated after the drilling phase for the production phase. The relocated ditch will carry less flow during the production phase but will be left at the minimum USDCM depth to provide a conservative capacity.

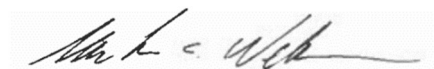
The Rational Method was used to compute peak flows draining into one offsite diversion ditch. The catchment area draining into Offsite Diversion Ditch 1 was found to be 16.28 acres with an imperviousness of 2% resulting in a 100-year flow rate of 21.48 cfs. Offsite Diversion Ditch 1 capable of conveying 24.32 cfs has been designed, with a 3:1 side slope, a minimum slope of 0.25%, a total depth of 1.25', and a bottom width of 5.0'. Offsite Diversion Ditch 1 will redirect offsite flows from Offsite Basin 1 around the site where it will be discharged west of the site and resume historic flow patterns.

The 23' wide access road is crowned with 1.25' deep swales along portions of each side. The swale on the east side of the access road within Offsite Basin 2 will collect a small amount of runoff and direct it to Culvert B where it will resume historic flow patterns. The swale on the east side of the access road within Offsite Basin 3 will collect a small amount of runoff and direct it to Culvert C where it will resume historic flow patterns. The swale on the south side of the access road within Offsite Basin 4 will collect a small amount of runoff and direct it to Culvert D where it will resume historic flow patterns.

Calculations for the diversion ditches, culverts, and riprap sizing are provided with this letter.

No adverse drainage impacts to the surrounding Site, properties, or floodplain resulting from the construction of the Site are anticipated. If the drainage patterns or imperviousness characteristics substantially deviate from what was considered in this drainage letter and the accompanying SWMP & Site Plan, the City of Aurora shall be notified. If you have any questions regarding the drainage associated with this project, please do not hesitate to call me at 303.928.7128.

Sincerely,



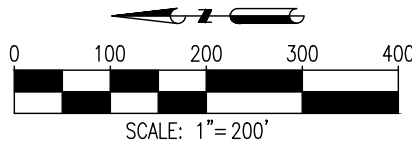
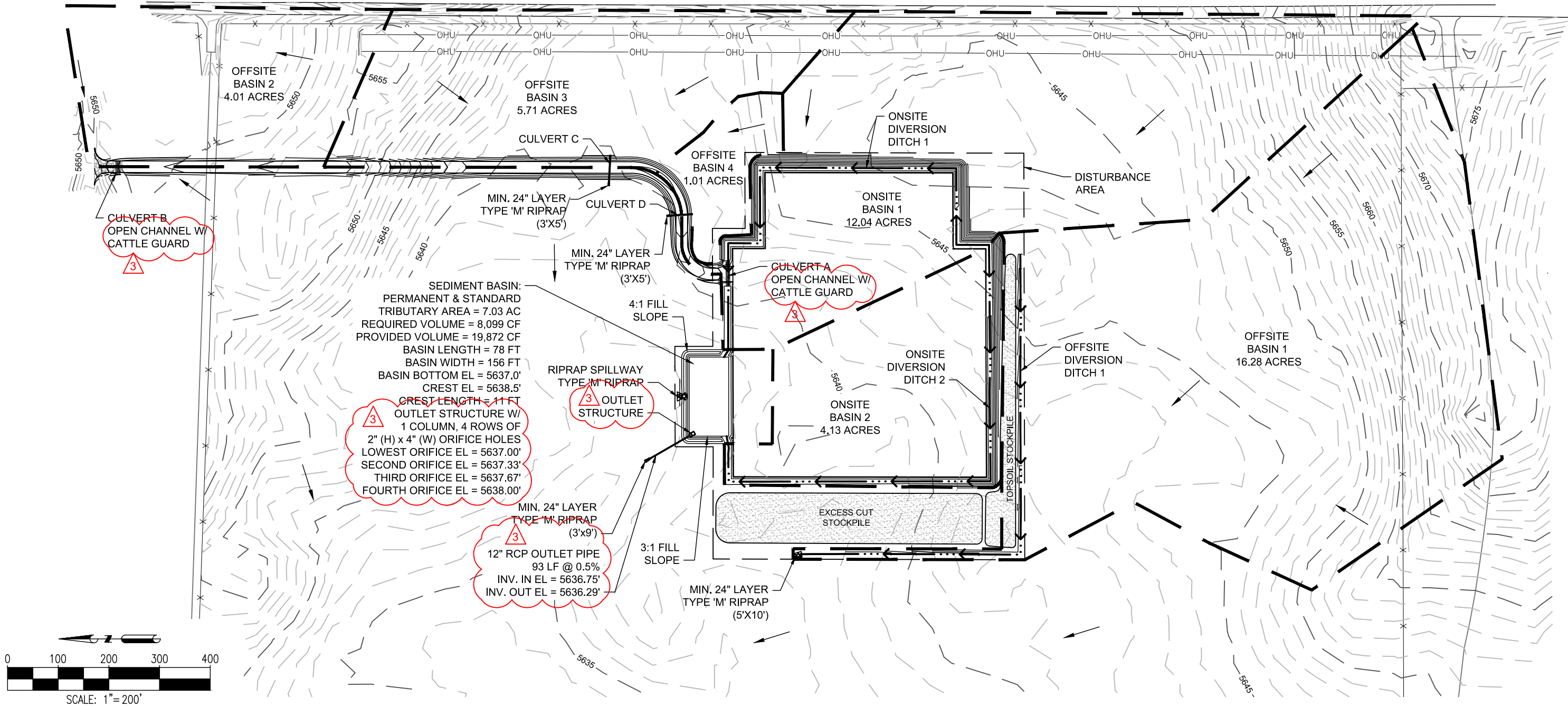
Michael Welker, PE, CFM  
Ascent Geomatics Solutions



# **Appendix A**

EASTERN HILLS SOUTH 4-65 17-18 3AH-3DH, 4AH-4DH PAD  
DRAINAGE BASIN BOUNDARY MAP

LEGEND  
--- = BASIN BOUNDARY  
---> = DIRECTION OF FLOW



DIG SAFELY  
BEFORE YOU DIG CALL:  
**1-800-922-1987**  
UTILITY NOTIFICATION  
CENTER OF COLORADO

This plot does not represent a monumented land survey and should not be relied upon to determine boundary lines, property ownership or other property interests. Parcel lines, if depicted have not been field verified and may be based upon publicly available data that also has not been independently verified.

DATA SOURCES:  
PUBLICLY AVAILABLE DATA SOURCES  
HAVE NOT BEEN INDEPENDENTLY  
VERIFIED BY ASCENT.



FIELD DATE: 02-15-18	SITE NAME: EASTERN HILLS SOUTH 4-65 17-18, 3AH-3DH, 4AH-4DH PAD
DRAWING DATE: 01-27-20	SURFACE LOCATION: E 1/2 SE 1/4 SEC. 17, T4S, R65W, 6TH P.M. ARAPAHOE COUNTY, COLORADO
BY: LM	CHECKED: DP

PREPARED FOR:  
**ConocoPhillips**

# National Flood Hazard Layer FIRMette



## Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT

SPECIAL FLOOD HAZARD AREAS

Without Base Flood Elevation (BFE)  
Zone A, V, A99

With BFE or Depth Zone AE, AO, AH, VE, AR

Regulatory Floodway

OTHER AREAS OF FLOOD HAZARD

0.2% Annual Chance Flood Hazard, Areas of 1% annual chance flood with average depth less than one foot or with drainage areas of less than one square mile Zone X

Future Conditions 1% Annual Chance Flood Hazard Zone X

Area with Reduced Flood Risk due to Levee. See Notes. Zone X

Area with Flood Risk due to Levee Zone D

OTHER AREAS

NO SCREEN

Effective LOMRs

Area of Undetermined Flood Hazard Zone D

GENERAL STRUCTURES

Channel, Culvert, or Storm Sewer

Levee, Dike, or Floodwall

OTHER FEATURES

20.2

17.5

Coastal Transect

Base Flood Elevation Line (BFE)

Limit of Study

Jurisdiction Boundary

Coastal Transect Baseline

Profile Baseline

Hydrographic Feature

MAP PANELS

Digital Data Available

No Digital Data Available

Unmapped

The pin displayed on the map is an approximate point selected by the user and does not represent an authoritative property location.



USGS The National Map: Orthoimagery. Data refreshed October 2017.

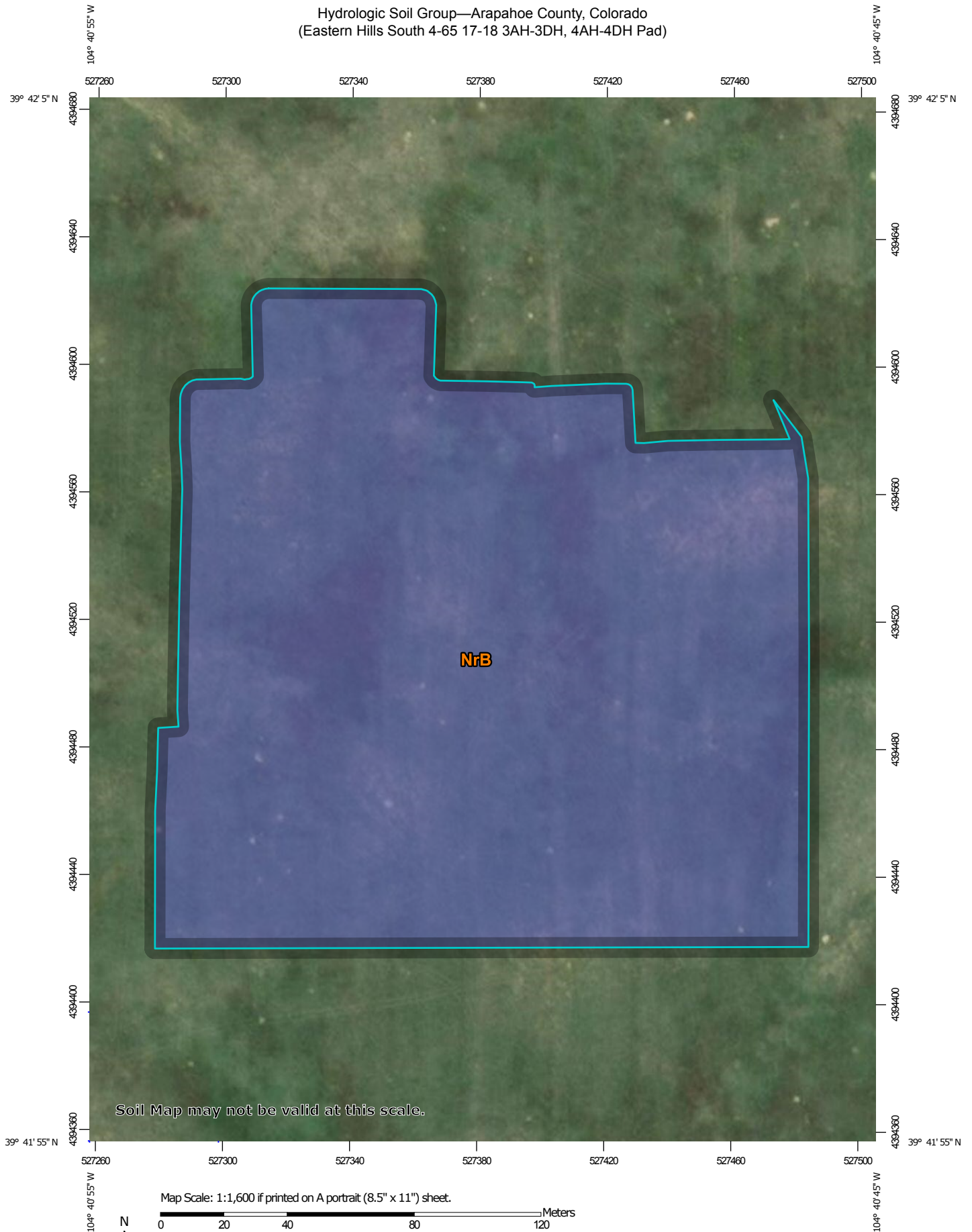
This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards

The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on **8/21/2018 at 5:46:30 PM** and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.



Hydrologic Soil Group—Arapahoe County, Colorado  
(Eastern Hills South 4-65 17-18 3AH-3DH, 4AH-4DH Pad)



## MAP LEGEND

### Area of Interest (AOI)

 Area of Interest (AOI)

### Soils

#### Soil Rating Polygons





 A  
 A/D  
 B  
 B/D  
 C  
 C/D  
 D  
 Not rated or not available

#### Soil Rating Lines


 A  
 A/D  
 B  
 B/D  
 C  
 C/D  
 D  
 Not rated or not available

#### Soil Rating Points

 A  
 A/D  
 B  
 B/D

 C  
 C/D  
 D  
 Not rated or not available


### Water Features

 Streams and Canals

### Transportation

 Rails  
 Interstate Highways  
 US Routes  
 Major Roads  
 Local Roads

### Background

 Aerial Photography

## MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:20,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service  
 Web Soil Survey URL:  
 Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Arapahoe County, Colorado  
 Survey Area Data: Version 14, Sep 10, 2018

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Jul 17, 2015—Oct 2, 2017

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

## Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
NrB	Nunn-Bresser-Ascalon complex, 0 to 3 percent slopes	B	9.0	100.0%
<b>Totals for Area of Interest</b>			<b>9.0</b>	<b>100.0%</b>

## Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

## Rating Options

*Aggregation Method:* Dominant Condition



*Component Percent Cutoff: None Specified*

*Tie-break Rule: Higher*

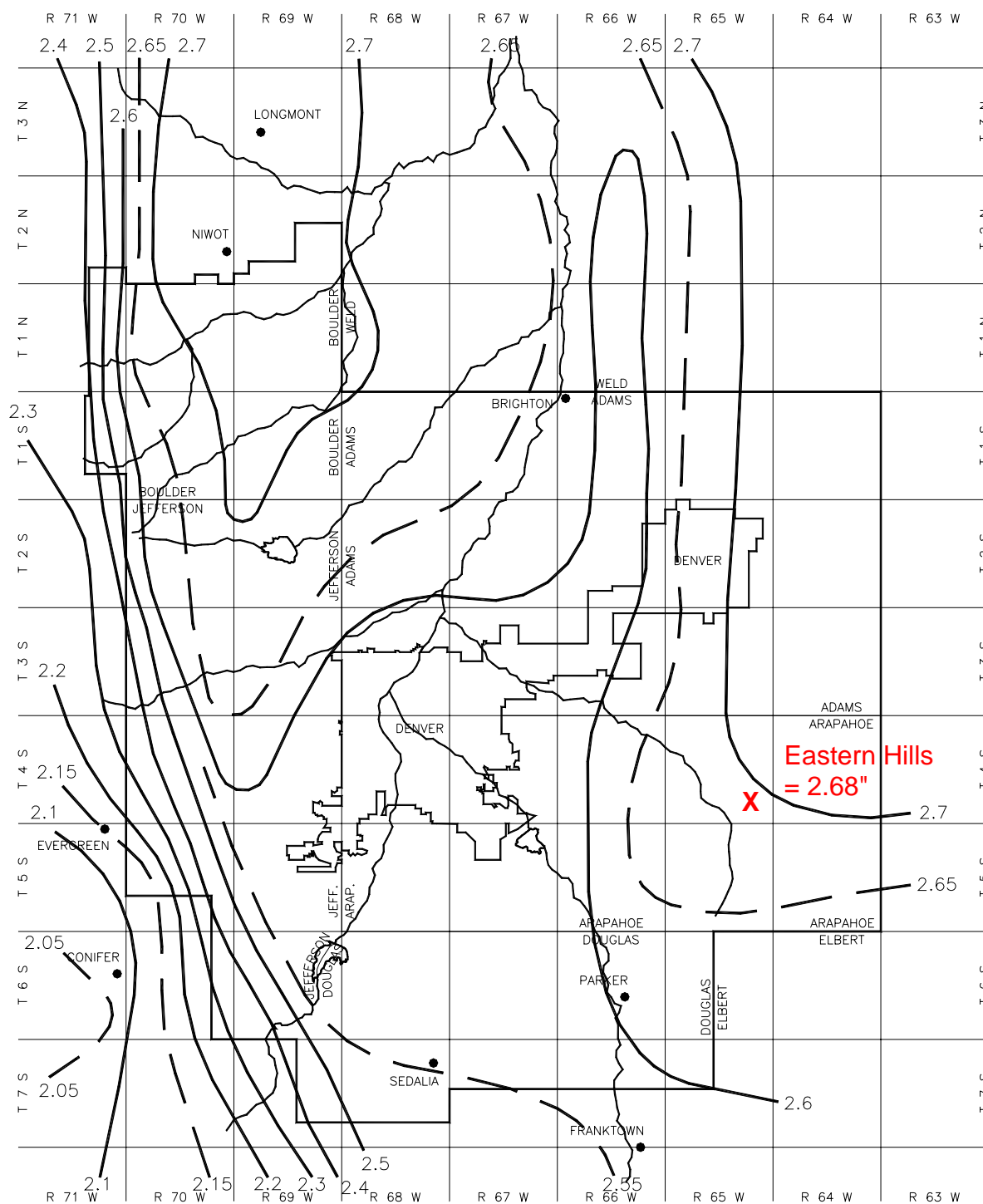


Figure RA-6—Rainfall Depth-Duration-Frequency: 100-Year, 1-Hour Rainfall

# Appendix B

## CALCULATION OF A PEAK RUNOFF USING RATIONAL METHOD

Project Title: **Eastern Hills South 4-65 17-18 3AH-3DH, 4AH-4DH Pad**  
 Catchment ID: **ONSITE BASIN 1**

### I. Catchment Hydrologic Data

Catchment ID = **ON-1**  
 Area = **12.04** Acres  
 Percent Imperviousness = **11.00** %  
 NRCS Soil Type = **B** A, B, C, or D

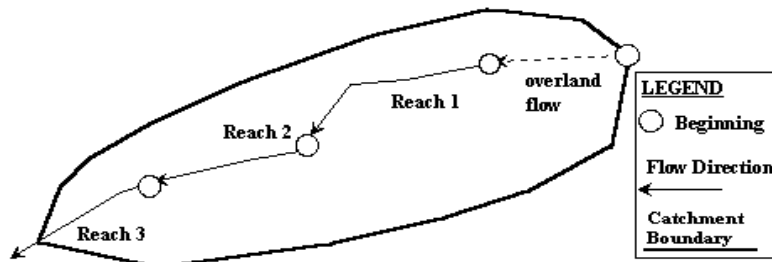
### II. Rainfall Information $I \text{ (inch/hr)} = C1 * P1 / (C2 + Td)^{C3}$

Design Storm Return Period,  $T_r$  = **100** years (input return period for design storm)  
 $C1$  = **28.50** (input the value of  $C1$ )  
 $C2$  = **10.00** (input the value of  $C2$ )  
 $C3$  = **0.786** (input the value of  $C3$ )  
 $P1$  = **2.68** inches (input one-hr precipitation--see Sheet "Design Info")

### III. Analysis of Flow Time (Time of Concentration) for a Catchment

Runoff Coefficient,  $C$  = **0.41**  
 Override Runoff Coefficient,  $C$  = (enter an override  $C$  value if desired, or leave blank to accept calculated  $C$ .)  
 5-yr. Runoff Coefficient,  $C-5$  = **0.14**  
 Override 5-yr. Runoff Coefficient,  $C$  = (enter an override  $C-5$  value if desired, or leave blank to accept calculated  $C-5$ .)

#### Illustration



NRCS Land Type	Heavy Meadow	Tillage/Field	Short Pasture/Lawns	Nearly Bare Ground	Grassed Swales/Waterways	Paved Areas & Shallow Paved Swales (Sheet Flow)
Conveyance	2.5	5	7	10	15	20

Calculations:

Reach ID	Slope S ft/ft input	Length L ft input	5-yr Runoff Coeff C-5 output	NRCS Conveyance input	Flow Velocity V fps output	Flow Time T <sub>f</sub> minutes output
Overland	0.0810	300	0.14	N/A	0.33	15.01
1	0.0120	1,511		10.00	1.10	22.99
2						
3						
4						
5						
Sum		1,811				
Computed T <sub>c</sub> =						37.99
Regional T <sub>c</sub> =						20.06
User-Entered T <sub>c</sub> =						38.59

### IV. Peak Runoff Prediction

Rainfall Intensity at Computed T<sub>c</sub>,  $I$  = **3.64** inch/hr  
 Rainfall Intensity at User-Defined T<sub>c</sub>,  $I$  = **3.61** inch/hr

Peak Flowrate,  $Q_p$  = **17.89** cfs  
 Peak Flowrate,  $Q_p$  = **17.72** cfs

## CALCULATION OF A PEAK RUNOFF USING RATIONAL METHOD

Project Title: Eastern Hills South 4-65 17-18 3AH-3DH, 4AH-4DH Pad  
 Catchment ID: ONSITE BASIN 2

### I. Catchment Hydrologic Data

Catchment ID = ON-2  
 Area = 4.13 Acres  
 Percent Imperviousness = 35.00 %  
 NRCS Soil Type = B A, B, C, or D

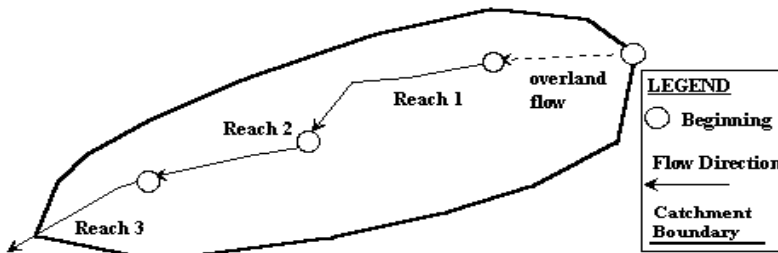
### II. Rainfall Information $I \text{ (inch/hr)} = C1 * P1 / (C2 + Td)^{C3}$

Design Storm Return Period,  $T_r$  = 100 years (input return period for design storm)  
 $C1$  = 28.50 (input the value of  $C1$ )  
 $C2$  = 10.00 (input the value of  $C2$ )  
 $C3$  = 0.786 (input the value of  $C3$ )  
 $P1$  = 2.68 inches (input one-hr precipitation--see Sheet "Design Info")

### III. Analysis of Flow Time (Time of Concentration) for a Catchment

Runoff Coefficient,  $C$  = 0.48  
 Override Runoff Coefficient,  $C$  = (enter an override  $C$  value if desired, or leave blank to accept calculated  $C$ .)  
 5-yr. Runoff Coefficient,  $C-5$  = 0.27  
 Override 5-yr. Runoff Coefficient,  $C$  = (enter an override  $C-5$  value if desired, or leave blank to accept calculated  $C-5$ .)

#### Illustration



NRCS Land Type	Heavy Meadow	Tillage/Field	Short Pasture/Lawns	Nearly Bare Ground	Grassed Swales/Waterways	Paved Areas & Shallow Paved Swales (Sheet Flow)
Conveyance	2.5	5	7	10	15	20

Calculations:

Reach ID	Slope S ft/ft input	Length L ft input	5-yr Runoff Coeff C-5 output	NRCS Conveyance input	Flow Velocity V fps output	Flow Time T <sub>f</sub> minutes output
Overland	0.3300	22	0.27	N/A	0.17	2.21
1	0.0011	1,082		10.00	0.33	54.37
2						
3						
4						
5						
Sum		1,104				
Computed T <sub>c</sub> =						56.58
Regional T <sub>c</sub> =						16.13
User-Entered T <sub>c</sub> =						16.13

### IV. Peak Runoff Prediction

Rainfall Intensity at Computed T<sub>c</sub>,  $I$  = 2.82 inch/hr  
 Rainfall Intensity at User-Defined T<sub>c</sub>,  $I$  = 5.88 inch/hr

Peak Flowrate,  $Q_p$  = 5.61 cfs  
 Peak Flowrate,  $Q_p$  = 11.70 cfs

## CALCULATION OF A PEAK RUNOFF USING RATIONAL METHOD

Project Title: **Eastern Hills South 4-65 17-18 3AH-3DH, 4AH-4DH Pad**  
 Catchment ID: **OFFSITE BASIN 1**

### I. Catchment Hydrologic Data

Catchment ID = **OFF-1**  
 Area = **16.28** Acres  
 Percent Imperviousness = **2.00** %  
 NRCS Soil Type = **B** A, B, C, or D

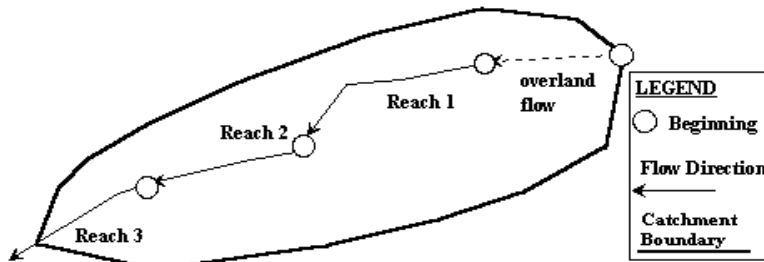
### II. Rainfall Information $I \text{ (inch/hr)} = C1 * P1 / (C2 + Td)^{C3}$

Design Storm Return Period,  $T_r$  = **100** years (input return period for design storm)  
 $C1$  = **28.50** (input the value of  $C1$ )  
 $C2$  = **10.00** (input the value of  $C2$ )  
 $C3$  = **0.786** (input the value of  $C3$ )  
 $P1$  = **2.68** inches (input one-hr precipitation--see Sheet "Design Info")

### III. Analysis of Flow Time (Time of Concentration) for a Catchment

Runoff Coefficient,  $C$  = **0.36**  
 Override Runoff Coefficient,  $C$  = (enter an override  $C$  value if desired, or leave blank to accept calculated  $C$ .)  
 5-yr. Runoff Coefficient,  $C-5$  = **0.08**  
 Override 5-yr. Runoff Coefficient,  $C$  = (enter an override  $C-5$  value if desired, or leave blank to accept calculated  $C-5$ .)

#### Illustration



NRCS Land Type	Heavy Meadow	Tillage/Field	Short Pasture/Lawns	Nearly Bare Ground	Grassed Swales/Waterways	Paved Areas & Shallow Paved Swales (Sheet Flow)
Conveyance	2.5	5	7	10	15	20

Calculations:

Reach ID	Slope S ft/ft input	Length L ft input	5-yr Runoff Coeff C-5 output	NRCS Conveyance input	Flow Velocity V fps output	Flow Time T <sub>f</sub> minutes output
Overland	0.0690	300	0.08	N/A	0.30	16.84
1	0.0130	1,376		10.00	1.14	20.11
2						
3						
4						
5						
Sum		1,676				
Computed T <sub>c</sub> =						36.95
Regional T <sub>c</sub> =						19.31
User-Entered T <sub>c</sub> =						38.02

### IV. Peak Runoff Prediction

Rainfall Intensity at Computed T<sub>c</sub>,  $I$  = **3.71** inch/hr  
 Rainfall Intensity at User-Defined T<sub>c</sub>,  $I$  = **3.64** inch/hr

Peak Flowrate,  $Q_p$  = **21.86** cfs  
 Peak Flowrate,  $Q_p$  = **21.48** cfs

## CALCULATION OF A PEAK RUNOFF USING RATIONAL METHOD

Project Title: **Eastern Hills South 4-65 17-18 3AH-3DH, 4AH-4DH Pad**  
 Catchment ID: **OFFSITE BASIN 2**

### I. Catchment Hydrologic Data

Catchment ID = **OFF-2**  
 Area = **4.01** Acres  
 Percent Imperviousness = **3.00** %  
 NRCS Soil Type = **B** A, B, C, or D

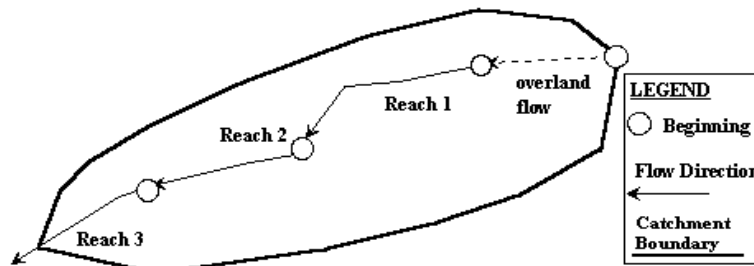
### II. Rainfall Information $I \text{ (inch/hr)} = C1 * P1 / (C2 + Td)^{C3}$

Design Storm Return Period,  $T_r$  = **100** years (input return period for design storm)  
 $C1$  = **28.50** (input the value of  $C1$ )  
 $C2$  = **10.00** (input the value of  $C2$ )  
 $C3$  = **0.786** (input the value of  $C3$ )  
 $P1$  = **2.68** inches (input one-hr precipitation--see Sheet "Design Info")

### III. Analysis of Flow Time (Time of Concentration) for a Catchment

Runoff Coefficient,  $C$  = **0.37**  
 Override Runoff Coefficient,  $C$  = (enter an override  $C$  value if desired, or leave blank to accept calculated  $C$ .)  
 5-yr. Runoff Coefficient,  $C-5$  = **0.08**  
 Override 5-yr. Runoff Coefficient,  $C$  = (enter an override  $C-5$  value if desired, or leave blank to accept calculated  $C-5$ .)

#### Illustration



NRCS Land Type	Heavy Meadow	Tillage/Field	Short Pasture/Lawns	Nearly Bare Ground	Grassed Swales/Waterways	Paved Areas & Shallow Paved Swales (Sheet Flow)
Conveyance	2.5	5	7	10	15	20

Calculations:

Reach ID	Slope S ft/ft input	Length L ft input	5-yr Runoff Coeff C-5 output	NRCS Conveyance input	Flow Velocity V fps output	Flow Time T <sub>f</sub> minutes output
Overland	0.020	35	0.08	N/A	0.07	8.63
1	0.007	402		15.00	1.25	5.34
2						
3						
4						
5						
Sum		437				
Computed T <sub>c</sub> =						13.96
Regional T <sub>c</sub> =						12.43
User-Entered T <sub>c</sub> =						12.43

### IV. Peak Runoff Prediction

Rainfall Intensity at Computed T<sub>c</sub>,  $I$  = **6.29** inch/hr  
 Rainfall Intensity at User-Defined T<sub>c</sub>,  $I$  = **6.63** inch/hr

Peak Flowrate,  $Q_p$  = **9.28** cfs  
 Peak Flowrate,  $Q_p$  = **9.78** cfs



## CALCULATION OF A PEAK RUNOFF USING RATIONAL METHOD

Project Title: **Eastern Hills South 4-65 17-18 3AH-3DH, 4AH-4DH Pad**  
 Catchment ID: **OFFSITE BASIN 3**

### I. Catchment Hydrologic Data

Catchment ID = **OFF-3**  
 Area = **5.71** Acres  
 Percent Imperviousness = **3.00** %  
 NRCS Soil Type = **B** A, B, C, or D

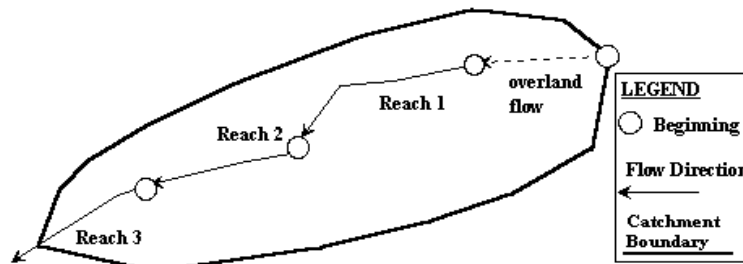
### II. Rainfall Information $I \text{ (inch/hr)} = C1 * P1 / (C2 + Td)^{C3}$

Design Storm Return Period,  $T_r$  = **100** years (input return period for design storm)  
 $C1$  = **28.50** (input the value of  $C1$ )  
 $C2$  = **10.00** (input the value of  $C2$ )  
 $C3$  = **0.786** (input the value of  $C3$ )  
 $P1$  = **2.68** inches (input one-hr precipitation--see Sheet "Design Info")

### III. Analysis of Flow Time (Time of Concentration) for a Catchment

Runoff Coefficient,  $C$  = **0.37**  
 Override Runoff Coefficient,  $C$  = (enter an override  $C$  value if desired, or leave blank to accept calculated  $C$ .)  
 5-yr. Runoff Coefficient,  $C-5$  = **0.08**  
 Override 5-yr. Runoff Coefficient,  $C$  = (enter an override  $C-5$  value if desired, or leave blank to accept calculated  $C-5$ .)

#### Illustration



NRCS Land Type	Heavy Meadow	Tillage/Field	Short Pasture/Lawns	Nearly Bare Ground	Grassed Swales/Waterways	Paved Areas & Shallow Paved Swales (Sheet Flow)
Conveyance	2.5	5	7	10	15	20

Calculations:

Reach ID	Slope S ft/ft input	Length L ft input	5-yr Runoff Coeff C-5 output	NRCS Conveyance input	Flow Velocity V fps output	Flow Time T <sub>f</sub> minutes output
Overland	0.0350	300	0.08	N/A	0.24	20.99
1	0.0050	235		10.00	0.71	5.54
2						
3						
4						
5						
Sum		535				
Computed T <sub>c</sub> =						26.53
Regional T <sub>c</sub> =						12.97
User-Entered T <sub>c</sub> =						28.06

### IV. Peak Runoff Prediction

Rainfall Intensity at Computed T<sub>c</sub>,  $I$  = **4.52** inch/hr  
 Rainfall Intensity at User-Defined T<sub>c</sub>,  $I$  = **4.37** inch/hr  
 Peak Flowrate,  $Q_p$  = **9.49** cfs  
 Peak Flowrate,  $Q_p$  = **9.19** cfs

## CALCULATION OF A PEAK RUNOFF USING RATIONAL METHOD

Project Title: **Eastern Hills South 4-65 17-18 3AH-3DH, 4AH-4DH Pad**  
 Catchment ID: **OFFSITE BASIN 4**

### I. Catchment Hydrologic Data

Catchment ID = **OFF-4**  
 Area = **1.01** Acres  
 Percent Imperviousness = **2.00** %  
 NRCS Soil Type = **B** A, B, C, or D

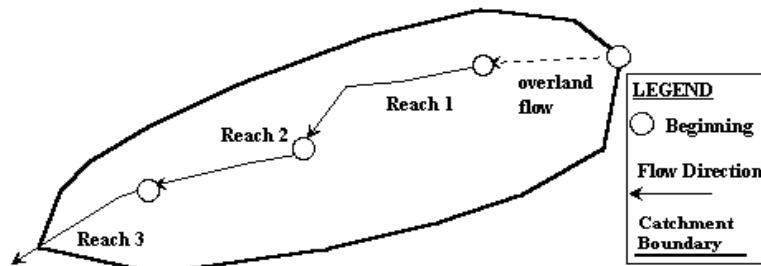
### II. Rainfall Information $I \text{ (inch/hr)} = C1 * P1 / (C2 + Td)^{C3}$

Design Storm Return Period,  $T_r$  = **100** years (input return period for design storm)  
 $C1$  = **28.50** (input the value of  $C1$ )  
 $C2$  = **10.00** (input the value of  $C2$ )  
 $C3$  = **0.786** (input the value of  $C3$ )  
 $P1$  = **2.68** inches (input one-hr precipitation--see Sheet "Design Info")

### III. Analysis of Flow Time (Time of Concentration) for a Catchment

Runoff Coefficient,  $C$  = **0.36**  
 Override Runoff Coefficient,  $C$  = (enter an override  $C$  value if desired, or leave blank to accept calculated  $C$ .)  
 5-yr. Runoff Coefficient,  $C-5$  = **0.08**  
 Override 5-yr. Runoff Coefficient,  $C$  = (enter an override  $C-5$  value if desired, or leave blank to accept calculated  $C-5$ .)

#### Illustration



NRCS Land Type	Heavy Meadow	Tillage/Field	Short Pasture/Lawns	Nearly Bare Ground	Grassed Swales/Waterways	Paved Areas & Shallow Paved Swales (Sheet Flow)
Conveyance	2.5	5	7	10	15	20

Calculations:

Reach ID	Slope S ft/ft input	Length L ft input	5-yr Runoff Coeff C-5 output	NRCS Conveyance input	Flow Velocity V fps output	Flow Time T <sub>f</sub> minutes output
Overland	0.020	292	0.08	N/A	0.19	25.00
1	0.0050	119		10.00	0.71	2.80
2						
3						
4						
5						
Sum		411				
Computed T <sub>c</sub> =						27.80
Regional T <sub>c</sub> =						12.28
User-Entered T <sub>c</sub> =						12.28

### IV. Peak Runoff Prediction

Rainfall Intensity at Computed T<sub>c</sub>,  $I$  = **4.40** inch/hr  
 Rainfall Intensity at User-Defined T<sub>c</sub>,  $I$  = **6.66** inch/hr

Peak Flowrate,  $Q_p$  = **1.61** cfs  
 Peak Flowrate,  $Q_p$  = **2.44** cfs

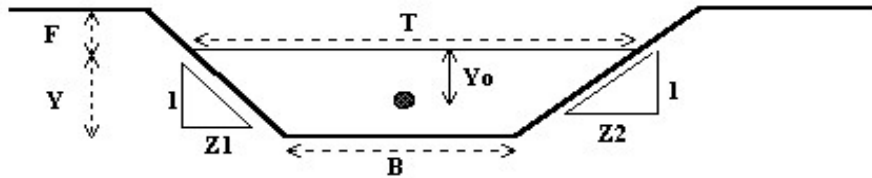
# Appendix C

## Normal Flow Analysis - Trapezoidal Channel

Project: **Eastern Hills South 4-65 17-18 3AH-3DH, 4AH-4DH Pad**

**Onsite Diversion Ditch 1**

Channel ID: **Design Flow = Q-100yr = 17.72 cfs (ON-1)**



### Design Information (Input)

Channel Invert Slope	$S_o =$ <u>0.0011</u> ft/ft
Manning's n	$n =$ <u>0.035</u>
Bottom Width	$B =$ <u>7.50</u> ft
Left Side Slope	$Z1 =$ <u>3.00</u> ft/ft
Right Side Slope	$Z2 =$ <u>3.00</u> ft/ft
Freeboard Height	$F =$ <u>0.00</u> ft
Design Water Depth	$Y =$ <u>1.25</u> ft

### Normal Flow Condition (Calculated)

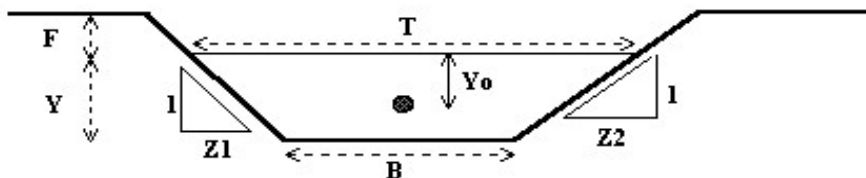
Discharge	$Q =$ <u>18.68</u> cfs
Froude Number	$Fr =$ <u>0.24</u>
Flow Velocity	$V =$ <u>1.33</u> fps
Flow Area	$A =$ <u>14.06</u> sq ft
Top Width	$T =$ <u>15.00</u> ft
Wetted Perimeter	$P =$ <u>15.41</u> ft
Hydraulic Radius	$R =$ <u>0.91</u> ft
Hydraulic Depth	$D =$ <u>0.94</u> ft
Specific Energy	$E_s =$ <u>1.28</u> ft
Centroid of Flow Area	$Y_o =$ <u>0.55</u> ft
Specific Force	$F_s =$ <u>0.53</u> kip

## Normal Flow Analysis - Trapezoidal Channel

Project: **Eastern Hills South 4-65 17-18 3AH-3DH, 4AH-4DH Pad**

**Onsite Diversion Ditch 2**

Channel ID: **Design Flow = Q-100yr = 11.70 cfs. (ON-2)**



### Design Information (Input)

Channel Invert Slope	$S_o =$ <u>0.0011</u> ft/ft
Manning's n	$n =$ <u>0.035</u>
Bottom Width	$B =$ <u>6.00</u> ft
Left Side Slope	$Z1 =$ <u>3.00</u> ft/ft
Right Side Slope	$Z2 =$ <u>3.00</u> ft/ft
Freeboard Height	$F =$ <u>0.00</u> ft
Design Water Depth	$Y =$ <u>1.25</u> ft

### Normal Flow Condition (Calculated)

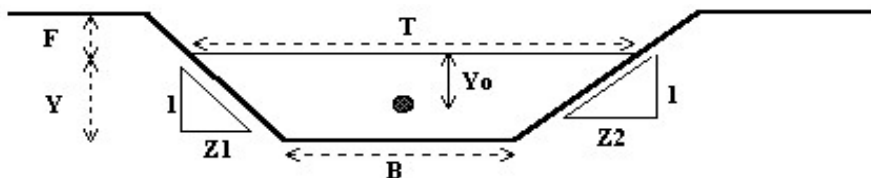
Discharge	$Q =$ <u>15.76</u> cfs
Froude Number	$Fr =$ <u>0.24</u>
Flow Velocity	$V =$ <u>1.29</u> fps
Flow Area	$A =$ <u>12.19</u> sq ft
Top Width	$T =$ <u>13.50</u> ft
Wetted Perimeter	$P =$ <u>13.91</u> ft
Hydraulic Radius	$R =$ <u>0.88</u> ft
Hydraulic Depth	$D =$ <u>0.90</u> ft
Specific Energy	$E_s =$ <u>1.28</u> ft
Centroid of Flow Area	$Y_o =$ <u>0.54</u> ft
Specific Force	$F_s =$ <u>0.45</u> kip

## Normal Flow Analysis - Trapezoidal Channel

Project: Eastern Hills South 4-65 17-18 3AH-3DH, 4AH-4DH Pad

Offsite Diversion Ditch 1

Channel ID: Design Flow = Q-100yr = 21.48 cfs. (OFF-1)



### Design Information (Input)

Channel Invert Slope	So = 0.0025 ft/ft
Manning's n	n = 0.030
Bottom Width	B = 5.00 ft
Left Side Slope	Z1 = 3.00 ft/ft
Right Side Slope	Z2 = 3.00 ft/ft
Freeboard Height	F = 0.00 ft
Design Water Depth	Y = 1.25 ft

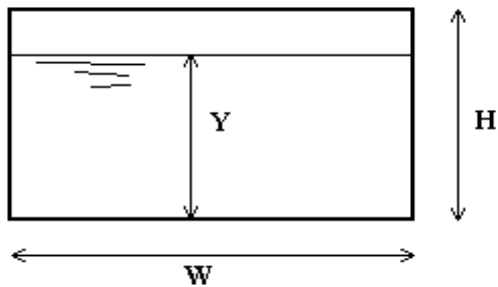
### Normal Flow Condition (Calculated)

Discharge	Q = 24.32 cfs
Froude Number	Fr = 0.42
Flow Velocity	V = 2.22 fps
Flow Area	A = 10.94 sq ft
Top Width	T = 12.50 ft
Wetted Perimeter	P = 12.91 ft
Hydraulic Radius	R = 0.85 ft
Hydraulic Depth	D = 0.88 ft
Specific Energy	Es = 1.33 ft
Centroid of Flow Area	Yo = 0.53 ft
Specific Force	Fs = 0.47 kip

## BOX CONDUIT FLOW (Normal & Critical Depth Computation)

Project: Eastern Hills South 4-65 17-18 3AH-3DH, 4AH-4DH Pad

Box ID: Culvert A - Open Channel w/ Cattle Guard (ON-1)



### Design Information (Input)

Box conduit invert slope	So =	0.0068	ft/ft
Box Manning's n-value	n =	0.0130	
Box Width	W =	7.50	ft
Box Height	H =	1.25	ft
Design discharge	Q =	17.72	cfs

### Full-flow capacity (Calculated)

Full-flow area	Af =	9.38	sq ft
Full-flow wetted perimeter	Pf =	17.50	ft
Full-flow capacity	Qf =	58.45	cfs

### Calculations of Normal Flow Condition

Normal flow depth ( $<H$ )	Yn =	0.46	ft
Flow area	An =	3.42	sq ft
Wetted perimeter	Pn =	8.41	ft
Flow velocity	Vn =	5.18	fps
Discharge	Qn =	17.72	cfs
Percent Full	Flow =	30.3%	of full flow
Normal Depth Froude Number	Fr <sub>n</sub> =	1.35	supercritical

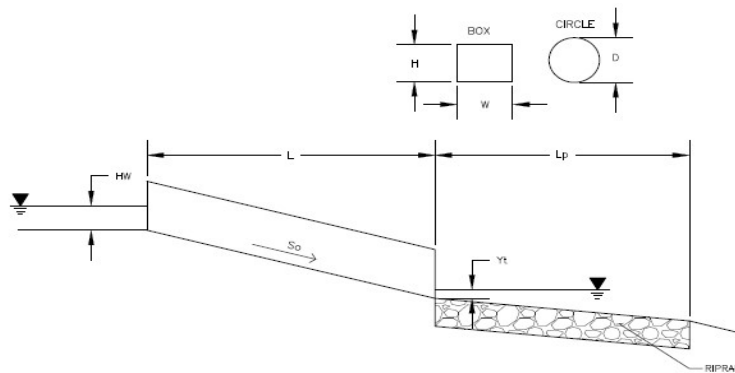
### Calculation of Critical Flow Condition

Critical flow depth	Yc =	0.56	ft
Critical flow area	Ac =	4.18	sq ft
Critical flow velocity	Vc =	4.24	fps
Critical Depth Froude Number	Fr <sub>c</sub> =	1.00	



# Determination of Culvert Headwater and Outlet Protection

Project: **Eastern Hills South 4-65 17-18 3AH-3DH, 4AH-4DH Pad**

Basin ID: **Culvert A**


## Soil Type:

Choose One:

☐ Sandy

☒ Non-Sandy

Supercritical Flow! Using Ha to calculate protection type.

## Design Information (Input):

Design Discharge

Q = 17.72 cfs

## Circular Culvert:

Barrel Diameter in Inches

D = inches

Inlet Edge Type (Choose from pull-down list)

Grooved End Projection

OR

Height (Rise) = 1.25 ft

Width (Span) = 7.5 ft

Square Edge w/ 90-15 Deg. Headwall

## Box Culvert:

Barrel Height (Rise) in Feet

Barrel Width (Span) in Feet

Inlet Edge Type (Choose from pull-down list)

Number of Barrels

No = 1

Inlet Elevation

Elev IN = 5638.28 ft

Outlet Elevation **OR** Slope

Elev OUT = 5637.95 ft

Culvert Length

L = 48.5 ft

Manning's Roughness

n = 0.013

Bend Loss Coefficient

k<sub>b</sub> = 0

Exit Loss Coefficient

k<sub>x</sub> = 1

Tailwater Surface Elevation

Elev Y<sub>t</sub> = ft

Max Allowable Channel Velocity

V = 7 ft/s

## Required Protection (Output):

Tailwater Surface Height

Y<sub>t</sub> = 0.50 ft

Flow Area at Max Channel Velocity

A<sub>t</sub> = 2.53 ft<sup>2</sup>

Culvert Cross Sectional Area Available

A = 9.38 ft<sup>2</sup>

Entrance Loss Coefficient

k<sub>e</sub> = 0.50

Friction Loss Coefficient

k<sub>f</sub> = 1.12

Sum of All Losses Coefficients

k<sub>s</sub> = 2.62

Culvert Normal Depth

Y<sub>n</sub> = 0.46 ft

Culvert Critical Depth

Y<sub>c</sub> = 0.56 ft

Tailwater Depth for Design

d = 0.90 ft

Adjusted Diameter **OR** Adjusted Rise

H<sub>a</sub> = 0.85 ft

Expansion Factor

1/(2\*tan(Θ)) = 6.65

Flow/Diameter<sup>2.5</sup> **OR** Flow/(Span \* Rise<sup>1.5</sup>)

Q/WH<sup>1.5</sup> = 1.69 ft<sup>0.5</sup>/s

Froude Number

Fr = 1.35

Tailwater/Adjusted Diameter **OR** Tailwater/Adjusted Rise

Y<sub>t</sub>/H = 0.59

Supercritical!

Inlet Control Headwater

HW<sub>i</sub> = 0.94 ft

Outlet Control Headwater

HW<sub>o</sub> = 0.72 ft

Design Headwater Elevation

HW = 5,639.22 ft

Headwater/Diameter **OR** Headwater/Rise Ratio

HW/H = 0.75

Minimum Theoretical Riprap Size

d<sub>50</sub> = 1 in

Nominal Riprap Size

d<sub>50</sub> = 6 in

UDFCD Riprap Type

Type = VL

Length of Protection

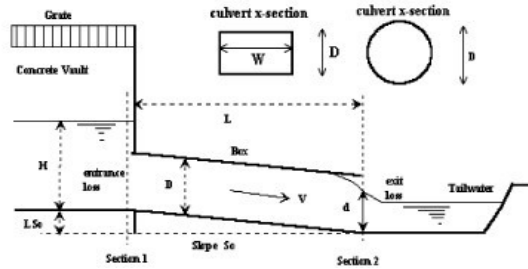
L<sub>p</sub> = 4 ft

Width of Protection

T = 9 ft

# CULVERT STAGE-DISCHARGE SIZING (INLET vs. OUTLET CONTROL WITH TAILWATER EFFECTS)

Project: **Eastern Hills South 4-65 17-18 3AH-3DH, 4AH-4DH Pad**  
 Basin ID: **Culvert A**  
 Status:



## Design Information (Input):

**Circular Culvert:** Barrel Diameter in Inches  
 Inlet Edge Type (choose from pull-down list)

D =  inches  
 Grooved End Projection

OR:

**Box Culvert:** Barrel Height (Rise) in Feet  
 Barrel Width (Span) in Feet  
 Inlet Edge Type (choose from pull-down list)

Height (Rise) =  1.25 ft.  
 Width (Span) =  7.5 ft.  
 Square Edge w/ 90-15 Deg. Headwall

Number of Barrels  
 Inlet Elevation at Culvert Invert  
 Outlet Elevation at Culvert Invert **OR** Slope of Culvert (ft v./ft h.)  
 Culvert Length in Feet  
 Manning's Roughness  
 Bend Loss Coefficient  
 Exit Loss Coefficient

No =  1  
 Inlet Elev =  5638.28 ft. elev.  
 Outlet Elev =  5637.95 ft. elev.  
 L =  48.5 ft.  
 n =  0.013  
 K<sub>b</sub> =  0  
 K<sub>x</sub> =  1

## Design Information (calculated):

Entrance Loss Coefficient  
 Friction Loss Coefficient  
 Sum of All Loss Coefficients  
 Orifice Inlet Condition Coefficient  
 Minimum Energy Condition Coefficient

K<sub>e</sub> =  0.50  
 K<sub>f</sub> =  1.12  
 K<sub>s</sub> =  2.62  
 C<sub>d</sub> =  0.83  
 K<sub>E<sub>low</sub></sub> =  0.3969

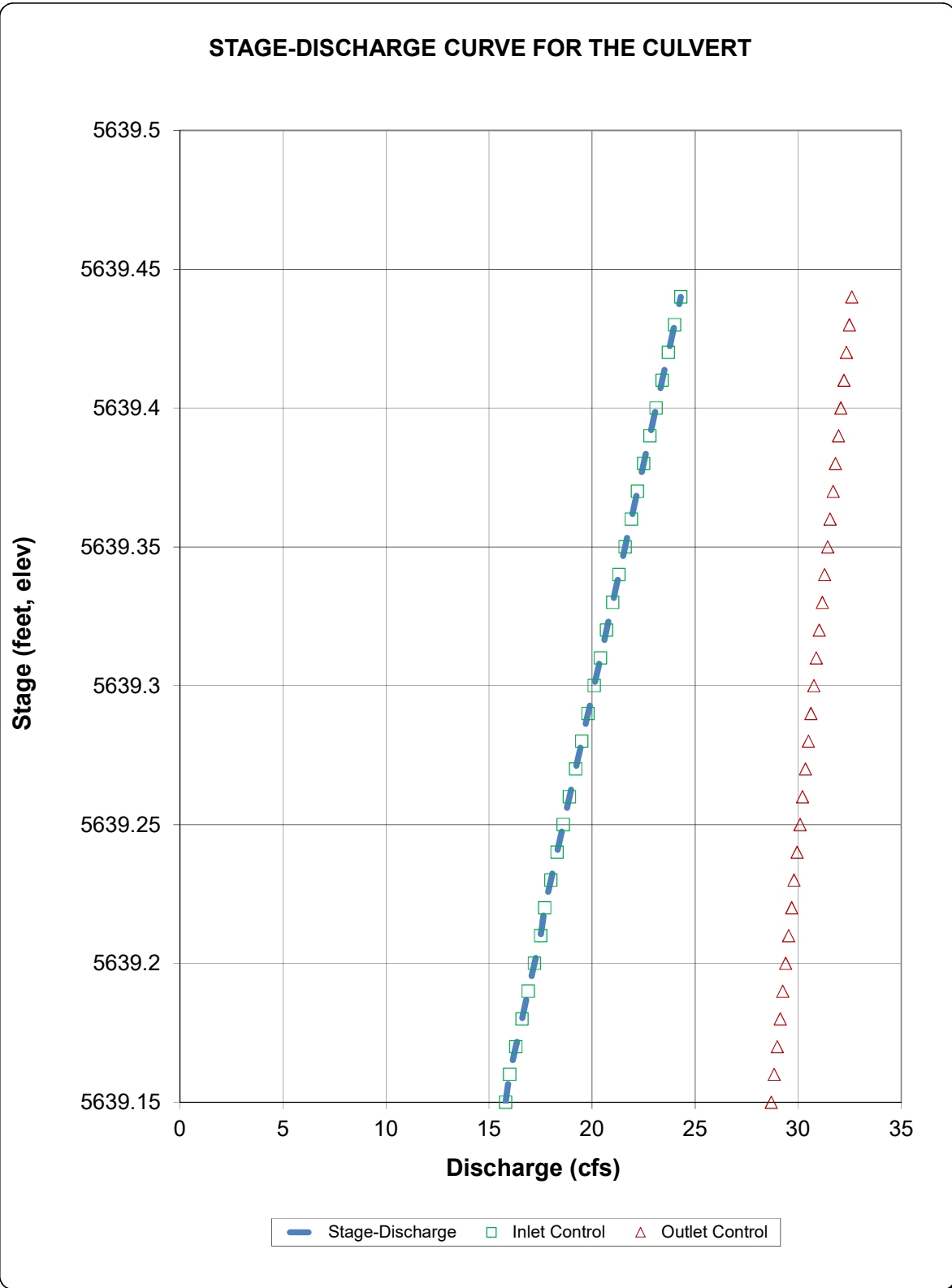
## Calculations of Culvert Capacity (output):

Water Surface Elevation (ft., linked)	Tailwater Surface Elevation ft	Culvert Inlet-Control Flowrate cfs	Culvert Outlet-Control Flowrate cfs	Controlling Culvert Flowrate cfs (output)	Inlet Equation Used:	Flow Control Used
5639.15		15.80	28.69	15.80	Regression Eqn.	INLET
5639.16		16.00	28.83	16.00	Regression Eqn.	INLET
5639.17		16.30	28.98	16.30	Regression Eqn.	INLET
5639.18		16.60	29.12	16.60	Regression Eqn.	INLET
5639.19		16.90	29.24	16.90	Regression Eqn.	INLET
5639.20		17.20	29.39	17.20	Regression Eqn.	INLET
5639.21		17.50	29.53	17.50	Regression Eqn.	INLET
5639.22		17.70	29.68	17.70	Regression Eqn.	INLET
5639.23		18.00	29.80	18.00	Regression Eqn.	INLET
5639.24		18.30	29.94	18.30	Regression Eqn.	INLET
5639.25		18.60	30.09	18.60	Regression Eqn.	INLET
5639.26		18.90	30.20	18.90	Regression Eqn.	INLET
5639.27		19.20	30.35	19.20	Regression Eqn.	INLET
5639.28		19.50	30.49	19.50	Regression Eqn.	INLET
5639.29		19.80	30.61	19.80	Regression Eqn.	INLET
5639.30		20.10	30.76	20.10	Regression Eqn.	INLET
5639.31		20.40	30.87	20.40	Regression Eqn.	INLET
5639.32		20.70	31.02	20.70	Regression Eqn.	INLET
5639.33		21.00	31.17	21.00	Regression Eqn.	INLET
5639.34		21.30	31.28	21.30	Regression Eqn.	INLET
5639.35		21.60	31.43	21.60	Regression Eqn.	INLET
5639.36		21.90	31.54	21.90	Regression Eqn.	INLET
5639.37		22.20	31.69	22.20	Regression Eqn.	INLET
5639.38		22.50	31.81	22.50	Regression Eqn.	INLET
5639.39		22.80	31.95	22.80	Regression Eqn.	INLET
5639.40		23.10	32.07	23.10	Regression Eqn.	INLET
5639.41		23.40	32.21	23.40	Regression Eqn.	INLET
5639.42		23.70	32.33	23.70	Regression Eqn.	INLET
5639.43		24.00	32.48	24.00	Regression Eqn.	INLET
5639.44		24.30	32.59	24.30	Regression Eqn.	INLET

Processing Time: 01.05 Seconds

## CULVERT STAGE-DISCHARGE SIZING (INLET vs. OUTLET CONTROL WITH TAILWATER EFFECTS)

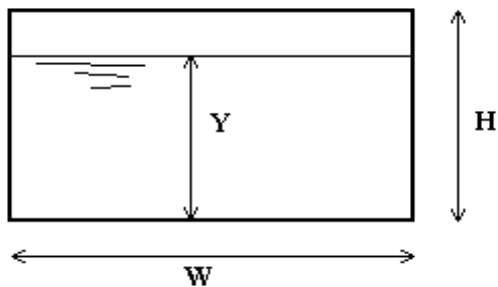
Project: Eastern Hills South 4-65 17-18 3AH-3DH, 4AH-4DH Pad  
Basin ID: Culvert A



## BOX CONDUIT FLOW (Normal & Critical Depth Computation)

Project: Eastern Hills South 4-65 17-18 3AH-3DH, 4AH-4DH Pad

Box ID: Culvert B - Open Channel w/ Culvert Cattle Guard (OFF-2)



### Design Information (Input)

Box conduit invert slope	$S_o =$	0.024	ft/ft
Box Manning's n-value	$n =$	0.0130	
Box Width	$W =$	7.00	ft
Box Height	$H =$	1.00	ft
<b>Design discharge</b>	<b><math>Q =</math></b>	<b>9.78</b>	<b>cfs</b>

### Full-flow capacity (Calculated)

Full-flow area	$A_f =$	7.00	sq ft
Full-flow wetted perimeter	$P_f =$	16.00	ft
Full-flow capacity	$Q_f =$	71.63	cfs

### Calculations of Normal Flow Condition

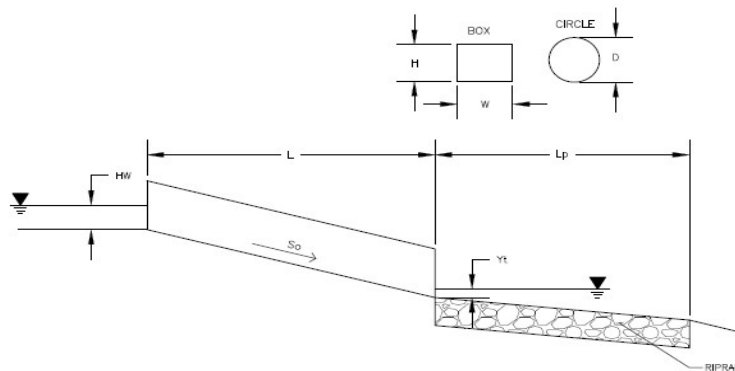
Normal flow depth ( $< H$ )	$Y_n =$	0.22	ft
Flow area	$A_n =$	1.56	sq ft
Wetted perimeter	$P_n =$	7.45	ft
Flow velocity	$V_n =$	6.27	fps
Discharge	$Q_n =$	9.78	cfs
Percent Full	Flow =	13.7%	of full flow
Normal Depth Froude Number	$Fr_n =$	2.34	supercritical

### Calculation of Critical Flow Condition

Critical flow depth	$Y_c =$	0.39	ft
Critical flow area	$A_c =$	2.75	sq ft
Critical flow velocity	$V_c =$	3.56	fps
Critical Depth Froude Number	$Fr_c =$	1.00	

# Determination of Culvert Headwater and Outlet Protection

Project: **Eastern Hills South 4-65 17-18 3AH-3DH, 4AH-4DH Pad**

Basin ID: **Culvert B**


## Soil Type:

Choose One:

☐ Sandy

☒ Non-Sandy

Supercritical Flow! Using Ha to calculate protection type.

## Design Information (Input):

Design Discharge

Q = 9.78 cfs

## Circular Culvert:

Barrel Diameter in Inches

D = inches

Inlet Edge Type (Choose from pull-down list)

## Box Culvert:

Barrel Height (Rise) in Feet

Height (Rise) = 1 ft

Barrel Width (Span) in Feet

Width (Span) = 7 ft

Inlet Edge Type (Choose from pull-down list)

Square Edge w/ 90-15 Deg. Headwall

Number of Barrels

No = 1

Inlet Elevation

Elev IN = 5650.81 ft

Outlet Elevation **OR** Slope

Elev OUT = 5650.21 ft

Culvert Length

L = 25.5 ft

Manning's Roughness

n = 0.013

Bend Loss Coefficient

k<sub>b</sub> = 0

Exit Loss Coefficient

k<sub>x</sub> = 1

Tailwater Surface Elevation

Elev Y<sub>t</sub> = ft

Max Allowable Channel Velocity

V = 7 ft/s

## Required Protection (Output):

Tailwater Surface Height

Y<sub>t</sub> = 0.40 ft

Flow Area at Max Channel Velocity

A<sub>t</sub> = 1.40 ft<sup>2</sup>

Culvert Cross Sectional Area Available

A = 7.00 ft<sup>2</sup>

Entrance Loss Coefficient

k<sub>e</sub> = 0.50

Friction Loss Coefficient

k<sub>f</sub> = 0.79

Sum of All Losses Coefficients

k<sub>s</sub> = 2.29

Culvert Normal Depth

Y<sub>n</sub> = 0.22 ft

Culvert Critical Depth

Y<sub>c</sub> = 0.39 ft

Tailwater Depth for Design

d = 0.70 ft

Adjusted Diameter **OR** Adjusted Rise

H<sub>a</sub> = 0.61 ft

Expansion Factor

1/(2\*tan(Θ)) = 6.65

Flow/Diameter<sup>2.5</sup> **OR** Flow/(Span \* Rise<sup>1.5</sup>)

Q/WH<sup>1.5</sup> = 1.40 ft<sup>0.5</sup>/s

Froude Number

Fr = 2.32

Tailwater/Adjusted Diameter **OR** Tailwater/Adjusted Rise

Y<sub>t</sub>/H = 0.65

Supercritical!

Inlet Control Headwater

HW<sub>i</sub> = 0.66 ft

Outlet Control Headwater

HW<sub>o</sub> = 0.17 ft

Design Headwater Elevation

HW = 5,651.47 ft

Headwater/Diameter **OR** Headwater/Rise Ratio

HW/H = 0.66

Minimum Theoretical Riprap Size

d<sub>50</sub> = 0 in

Nominal Riprap Size

d<sub>50</sub> = 6 in

UDFCD Riprap Type

Type = VL

Length of Protection

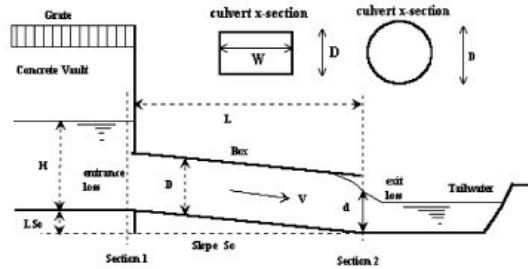
L<sub>p</sub> = 3 ft

Width of Protection

T = 8 ft

# CULVERT STAGE-DISCHARGE SIZING (INLET vs. OUTLET CONTROL WITH TAILWATER EFFECTS)

Project: **Eastern Hills 4-64 17-18 3AH-3DH, 4AH-4DH Pad**  
 Basin ID: **Culvert B**  
 Status:



## Design Information (Input):

**Circular Culvert:** Barrel Diameter in Inches  
 Inlet Edge Type (choose from pull-down list)

D =  inches  
 Grooved End with Headwall

OR:

**Box Culvert:** Barrel Height (Rise) in Feet  
 Barrel Width (Span) in Feet  
 Inlet Edge Type (choose from pull-down list)

Height (Rise) =  ft.  
 Width (Span) =  ft.  
 Square Edge w/ 0 deg. Flared Wingwall

Number of Barrels  
 Inlet Elevation at Culvert Invert  
 Outlet Elevation at Culvert Invert **OR** Slope of Culvert (ft v./ft h.)  
 Culvert Length in Feet  
 Manning's Roughness  
 Bend Loss Coefficient  
 Exit Loss Coefficient

No =   
 Inlet Elev =  ft. elev.  
 Outlet Elev =  ft. elev.  
 L =  ft.  
 n =   
 K<sub>b</sub> =   
 K<sub>x</sub> =

## Design Information (calculated):

Entrance Loss Coefficient  
 Friction Loss Coefficient  
 Sum of All Loss Coefficients  
 Orifice Inlet Condition Coefficient  
 Minimum Energy Condition Coefficient

K<sub>e</sub> =   
 K<sub>f</sub> =   
 K<sub>s</sub> =   
 C<sub>d</sub> =   
 K<sub>E<sub>low</sub></sub> =

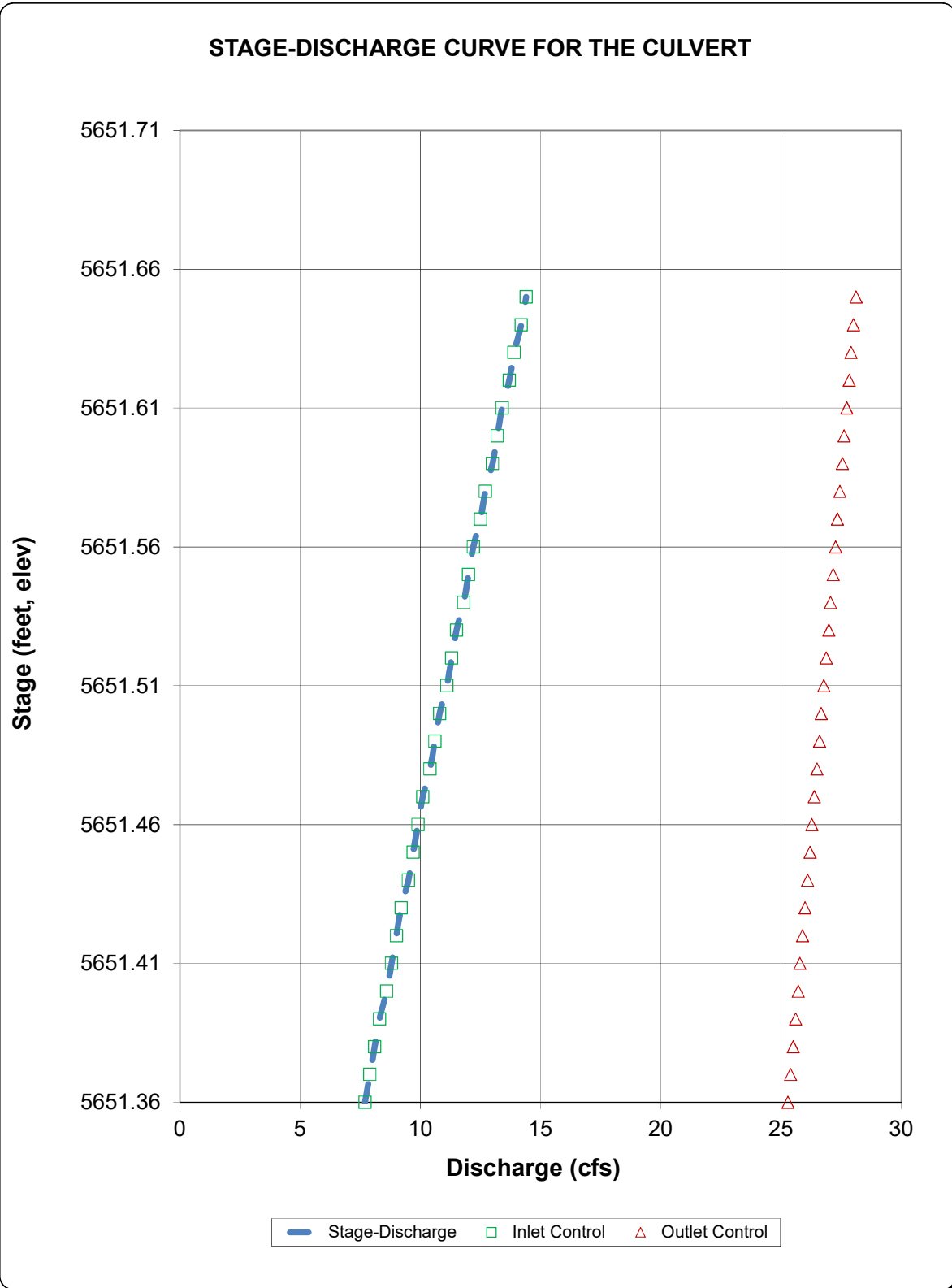
## Calculations of Culvert Capacity (output):

Water Surface Elevation (ft., linked)	Tailwater Surface Elevation ft	Culvert Inlet-Control Flowrate cfs	Culvert Outlet-Control Flowrate cfs	Controlling Culvert Flowrate cfs (output)	Inlet Equation Used:	Flow Control Used
5651.36		7.70	25.29	7.70	Regression Eqn.	INLET
5651.37		7.90	25.39	7.90	Regression Eqn.	INLET
5651.38		8.10	25.50	8.10	Regression Eqn.	INLET
5651.39		8.30	25.61	8.30	Regression Eqn.	INLET
5651.40		8.60	25.71	8.60	Regression Eqn.	INLET
5651.41		8.80	25.78	8.80	Regression Eqn.	INLET
5651.42		9.00	25.89	9.00	Regression Eqn.	INLET
5651.43		9.20	26.00	9.20	Regression Eqn.	INLET
5651.44		9.50	26.10	9.50	Regression Eqn.	INLET
5651.45		9.70	26.21	9.70	Regression Eqn.	INLET
5651.46		9.90	26.28	9.90	Regression Eqn.	INLET
5651.47		10.10	26.38	10.10	Regression Eqn.	INLET
5651.48		10.40	26.49	10.40	Regression Eqn.	INLET
5651.49		10.60	26.60	10.60	Regression Eqn.	INLET
5651.50		10.80	26.67	10.80	Regression Eqn.	INLET
5651.51		11.10	26.77	11.10	Regression Eqn.	INLET
5651.52		11.30	26.88	11.30	Regression Eqn.	INLET
5651.53		11.50	26.99	11.50	Regression Eqn.	INLET
5651.54		11.80	27.06	11.80	Regression Eqn.	INLET
5651.55		12.00	27.16	12.00	Regression Eqn.	INLET
5651.56		12.20	27.27	12.20	Regression Eqn.	INLET
5651.57		12.50	27.34	12.50	Regression Eqn.	INLET
5651.58		12.70	27.45	12.70	Regression Eqn.	INLET
5651.59		13.00	27.55	13.00	Regression Eqn.	INLET
5651.60		13.20	27.62	13.20	Regression Eqn.	INLET
5651.61		13.40	27.73	13.40	Regression Eqn.	INLET
5651.62		13.70	27.83	13.70	Regression Eqn.	INLET
5651.63		13.90	27.90	13.90	Regression Eqn.	INLET
5651.64		14.20	28.01	14.20	Regression Eqn.	INLET
5651.65		14.40	28.12	14.40	Regression Eqn.	INLET

Processing Time: 01.04 Seconds

## CULVERT STAGE-DISCHARGE SIZING (INLET vs. OUTLET CONTROL WITH TAILWATER EFFECTS)

Project: Eastern Hills 4-64 17-18 3AH-3DH, 4AH-4DH Pad  
Basin ID: Culvert B

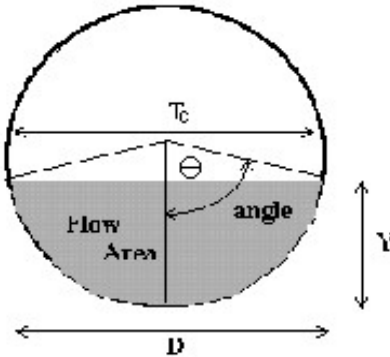




# CIRCULAR CONDUIT FLOW (Normal & Critical Depth Computation)

Project: Eastern Hills South 4-65 17-18 3AH-3DH, 4AH-4DH Pad

Pipe ID: Culvert C



## Design Information (Input)

Pipe Invert Slope	So =	0.0060	ft/ft
Pipe Manning's n-value	n =	0.0130	
Pipe Diameter	D =	24.00	inches
Design discharge	Q =	9.19	cfs

## Full-flow Capacity (Calculated)

Full-flow area	Af =	3.14	sq ft
Full-flow wetted perimeter	Pf =	6.28	ft
Half Central Angle	Theta =	3.14	radians
Full-flow capacity	Qf =	17.57	cfs

## Calculation of Normal Flow Condition

Half Central Angle ( $0 < \text{Theta} < 3.14$ )	Theta =	1.60	radians
Flow area	An =	1.62	sq ft
Top width	Tn =	2.00	ft
Wetted perimeter	Pn =	3.20	ft
Flow depth	Yn =	1.03	ft
Flow velocity	Vn =	5.66	fps
Discharge	Qn =	9.19	cfs
Percent Full Flow	Flow =	52.3%	of full flow
Normal Depth Froude Number	Fr <sub>n</sub> =	1.11	supercritical

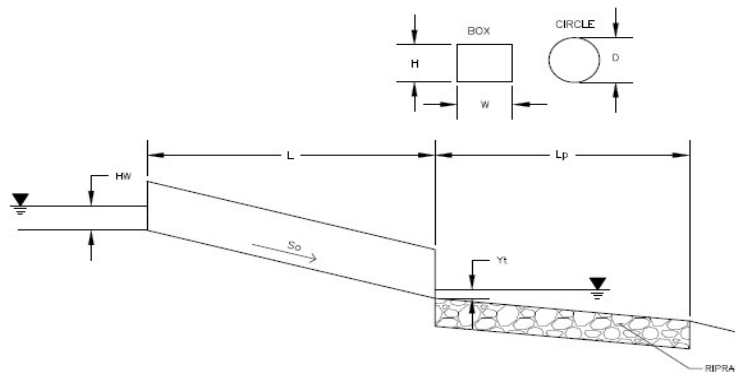
## Calculation of Critical Flow Condition

Half Central Angle ( $0 < \text{Theta-c} < 3.14$ )	Theta-c =	1.65	radians
Critical flow area	Ac =	1.74	sq ft
Critical top width	Tc =	1.99	ft
Critical flow depth	Yc =	1.08	ft
Critical flow velocity	Vc =	5.29	fps
Critical Depth Froude Number	Fr <sub>c</sub> =	1.00	

## Determination of Culvert Headwater and Outlet Protection

Project: **Eastern Hills South 4-65 17-18 3AH-3DH, 4AH-4DH Pad**

Basin ID: **Culvert C**



### Soil Type:

Choose One:

☐ Sandy

☒ Non-Sandy

Supercritical Flow! Using  $D_a$  to calculate protection type.

### Design Information (Input):

Design Discharge

Q = 9.19 cfs

### Circular Culvert:

Barrel Diameter in Inches

D = 24 inches

Inlet Edge Type (Choose from pull-down list)

Grooved End Projection

OR

### Box Culvert:

Barrel Height (Rise) in Feet

Height (Rise) = ft

Barrel Width (Span) in Feet

Width (Span) = ft

Inlet Edge Type (Choose from pull-down list)

Number of Barrels

No = 1

Inlet Elevation

Elev IN = 5639.90 ft

Outlet Elevation **OR** Slope

So = 0.006 ft/ft

Culvert Length

L = 55.0 ft

Manning's Roughness

n = 0.013

Bend Loss Coefficient

$k_b$  = 0

Exit Loss Coefficient

$k_x$  = 1

Tailwater Surface Elevation

Elev  $Y_t$  = ft

Max Allowable Channel Velocity

V = 7 ft/s

### Required Protection (Output):

Tailwater Surface Height

$Y_t$  = 0.80 ft

Flow Area at Max Channel Velocity

$A_t$  = 1.31  $\text{ft}^2$

Culvert Cross Sectional Area Available

A = 3.14  $\text{ft}^2$

Entrance Loss Coefficient

$k_e$  = 0.20

Friction Loss Coefficient

$k_f$  = 0.68

Sum of All Losses Coefficients

$k_s$  = 1.88

Culvert Normal Depth

$Y_n$  = 1.03 ft

Culvert Critical Depth

$Y_c$  = 1.08 ft

Tailwater Depth for Design

d = 1.54 ft

Adjusted Diameter **OR** Adjusted Rise

$D_a$  = 1.51 ft

Expansion Factor

$1/(2*\tan(\Theta))$  = 6.70

Flow/Diameter<sup>2.5</sup> **OR** Flow/(Span \* Rise<sup>1.5</sup>)

$Q/D^{2.5}$  = 1.62  $\text{ft}^{0.5}/\text{s}$

Froude Number

Fr = 1.11

Tailwater/Adjusted Diameter **OR** Tailwater/Adjusted Rise

$Y_t/D$  = 0.53

Supercritical!

Inlet Control Headwater

$HW_i$  = 1.55 ft

Outlet Control Headwater

$HW_o$  = 1.46 ft

Design Headwater Elevation

HW = 5.641.45 ft

Headwater/Diameter **OR** Headwater/Rise Ratio

$HW/D$  = 0.78

Minimum Theoretical Riprap Size

$d_{50}$  = 3 in

Nominal Riprap Size

$d_{50}$  = 6 in

UDFCD Riprap Type

Type = VL

Length of Protection

$L_p$  = 6 ft

Width of Protection

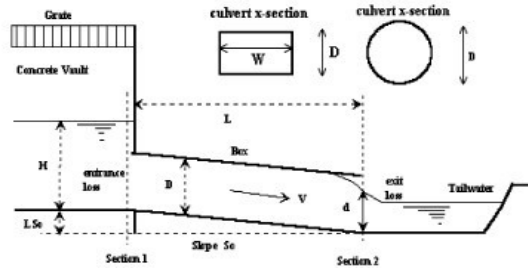
T = 3 ft

## CULVERT STAGE-DISCHARGE SIZING (INLET vs. OUTLET CONTROL WITH TAILWATER EFFECTS)

Project: **Eastern Hills South 4-65 17-18 3AH-3DH, 4AH-4DH Pad**

Basin ID: **Culvert C**

Status:



### Design Information (Input):

**Circular Culvert:** Barrel Diameter in Inches

Inlet Edge Type (choose from pull-down list)

$D =$   inches

**OR:**

**Box Culvert:** Barrel Height (Rise) in Feet

Barrel Width (Span) in Feet

Inlet Edge Type (choose from pull-down list)

Height (Rise) =  ft.

Width (Span) =  ft.

Number of Barrels

Inlet Elevation at Culvert Invert

Outlet Elevation at Culvert Invert **OR** Slope of Culvert (ft v./ft h.)

Culvert Length in Feet

Manning's Roughness

Bend Loss Coefficient

Exit Loss Coefficient

No =

Inlet Elev =  ft. elev.

Slope =  ft vert. / ft horiz.

$L =$   ft.

$n =$

$K_b =$

$K_x =$

### Design Information (calculated):

Entrance Loss Coefficient

Friction Loss Coefficient

Sum of All Loss Coefficients

Orifice Inlet Condition Coefficient

Minimum Energy Condition Coefficient

$K_e =$

$K_f =$

$K_s =$

$C_d =$

$KE_{low} =$

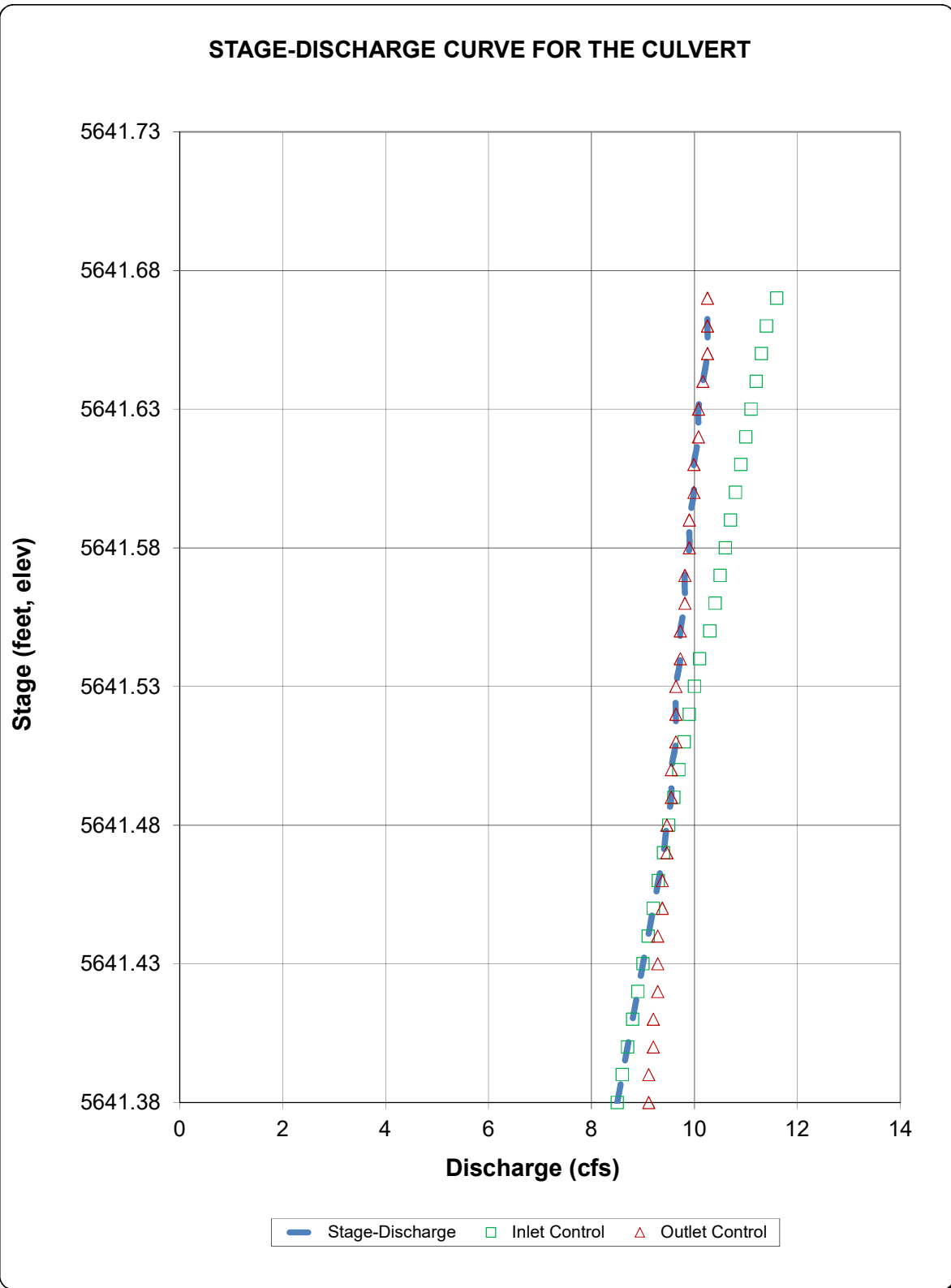
### Calculations of Culvert Capacity (output):

Water Surface Elevation (ft., linked)	Tailwater Surface Elevation ft	Culvert Inlet-Control Flowrate cfs	Culvert Outlet-Control Flowrate cfs	Controlling Culvert Flowrate cfs (output)	Inlet Equation Used:	Flow Control Used
5641.38		8.50	9.11	8.50	Regression Eqn.	INLET
5641.39		8.60	9.11	8.60	Regression Eqn.	INLET
5641.40		8.70	9.20	8.70	Regression Eqn.	INLET
5641.41		8.80	9.20	8.80	Regression Eqn.	INLET
5641.42		8.90	9.29	8.90	Regression Eqn.	INLET
5641.43		9.00	9.29	9.00	Regression Eqn.	INLET
5641.44		9.10	9.29	9.10	Regression Eqn.	INLET
5641.45		9.20	9.38	9.20	Regression Eqn.	INLET
5641.46		9.30	9.38	9.30	Regression Eqn.	INLET
5641.47		9.40	9.46	9.40	Regression Eqn.	INLET
5641.48		9.50	9.46	9.46	Regression Eqn.	OUTLET
5641.49		9.60	9.55	9.55	Regression Eqn.	OUTLET
5641.50		9.70	9.55	9.55	Regression Eqn.	OUTLET
5641.51		9.80	9.64	9.64	Regression Eqn.	OUTLET
5641.52		9.90	9.64	9.64	Regression Eqn.	OUTLET
5641.53		10.00	9.64	9.64	Regression Eqn.	OUTLET
5641.54		10.10	9.73	9.73	Regression Eqn.	OUTLET
5641.55		10.30	9.73	9.73	Regression Eqn.	OUTLET
5641.56		10.40	9.81	9.81	Regression Eqn.	OUTLET
5641.57		10.50	9.81	9.81	Regression Eqn.	OUTLET
5641.58		10.60	9.90	9.90	Regression Eqn.	OUTLET
5641.59		10.70	9.90	9.90	Regression Eqn.	OUTLET
5641.60		10.80	9.99	9.99	Regression Eqn.	OUTLET
5641.61		10.90	9.99	9.99	Regression Eqn.	OUTLET
5641.62		11.00	10.08	10.08	Regression Eqn.	OUTLET
5641.63		11.10	10.08	10.08	Regression Eqn.	OUTLET
5641.64		11.20	10.16	10.16	Regression Eqn.	OUTLET
5641.65		11.30	10.25	10.25	Regression Eqn.	OUTLET
5641.66		11.40	10.25	10.25	Regression Eqn.	OUTLET
5641.67		11.60	10.25	10.25	Regression Eqn.	OUTLET

Processing Time: 01.02 Seconds

## CULVERT STAGE-DISCHARGE SIZING (INLET vs. OUTLET CONTROL WITH TAILWATER EFFECTS)

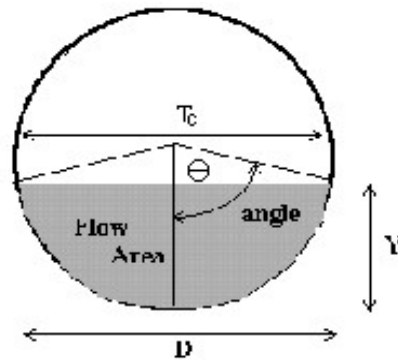
Project: Eastern Hills South 4-65 17-18 3AH-3DH, 4AH-4DH Pad  
Basin ID: Culvert C



## CIRCULAR CONDUIT FLOW (Normal & Critical Depth Computation)

Project: **Eastern Hills South 4-65 17-18 3AH-3DH, 4AH-4DH Pad**

Pipe ID: **Culvert D**



### Design Information (Input)

Pipe Invert Slope	So =	0.0130	ft/ft
Pipe Manning's n-value	n =	0.0130	
Pipe Diameter	D =	12.00	inches
Design discharge	Q =	2.44	cfs

### Full-flow Capacity (Calculated)

Full-flow area	Af =	0.79	sq ft
Full-flow wetted perimeter	Pf =	3.14	ft
Half Central Angle	Theta =	3.14	radians
Full-flow capacity	Qf =	4.07	cfs

### Calculation of Normal Flow Condition

Half Central Angle ( $0 < \text{Theta} < 3.14$ )	Theta =	1.69	radians
Flow area	An =	0.45	sq ft
Top width	Tn =	0.99	ft
Wetted perimeter	Pn =	1.69	ft
Flow depth	Yn =	0.56	ft
Flow velocity	Vn =	5.42	fps
Discharge	Qn =	2.44	cfs
Percent Full Flow	Flow =	60.0%	of full flow
Normal Depth Froude Number	Fr <sub>n</sub> =	1.42	supercritical

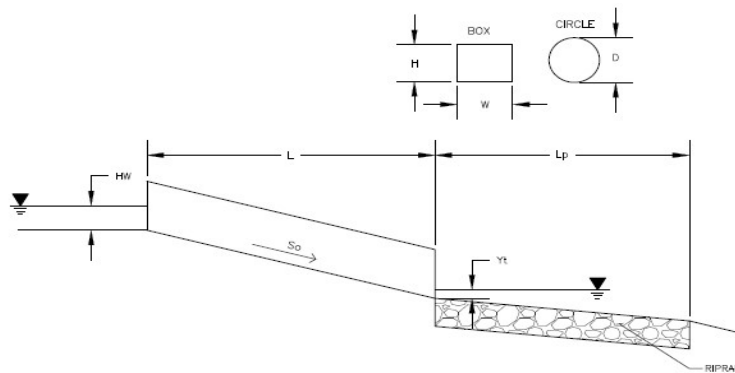
### Calculation of Critical Flow Condition

Half Central Angle ( $0 < \text{Theta-c} < 3.14$ )	Theta-c =	1.92	radians
Critical flow area	Ac =	0.56	sq ft
Critical top width	Tc =	0.94	ft
Critical flow depth	Yc =	0.67	ft
Critical flow velocity	Vc =	4.37	fps
Critical Depth Froude Number	Fr <sub>c</sub> =	1.00	

## Determination of Culvert Headwater and Outlet Protection

Project: **Eastern Hills South 4-65 17-18 3AH-3DH, 4AH-4DH Pad**

Basin ID: **Culvert D**



Soil Type:

Choose One:

☐ Sandy

☒ Non-Sandy

Supercritical Flow! Using  $D_a$  to calculate protection type.

### Design Information (Input):

Design Discharge

Q = 2.44 cfs

#### Circular Culvert:

Barrel Diameter in Inches

D = 12 inches

Inlet Edge Type (Choose from pull-down list)

Grooved End Projection

OR

#### Box Culvert:

Barrel Height (Rise) in Feet

Height (Rise) = ft

Barrel Width (Span) in Feet

Width (Span) = ft

Inlet Edge Type (Choose from pull-down list)

Number of Barrels

No = 1

Inlet Elevation

Elev IN = 5640.32 ft

Outlet Elevation **OR** Slope

Elev OUT = 5639.73 ft

Culvert Length

L = 45.5 ft

Manning's Roughness

n = 0.013

Bend Loss Coefficient

$k_b$  = 0

Exit Loss Coefficient

$k_x$  = 1

Tailwater Surface Elevation

Elev  $Y_t$  = ft

Max Allowable Channel Velocity

V = 7 ft/s

### Required Protection (Output):

Tailwater Surface Height

$Y_t$  = 0.40 ft

Flow Area at Max Channel Velocity

$A_t$  = 0.35 ft<sup>2</sup>

Culvert Cross Sectional Area Available

A = 0.79 ft<sup>2</sup>

Entrance Loss Coefficient

$k_e$  = 0.20

Friction Loss Coefficient

$k_f$  = 1.42

Sum of All Losses Coefficients

$k_s$  = 2.62

Culvert Normal Depth

$Y_n$  = 0.56 ft

Culvert Critical Depth

$Y_c$  = 0.67 ft

Tailwater Depth for Design

d = 0.83 ft

Adjusted Diameter **OR** Adjusted Rise

$D_a$  = 0.78 ft

Expansion Factor

$1/(2*\tan(\Theta))$  = 6.38

Flow/Diameter<sup>2.5</sup> **OR** Flow/(Span \* Rise<sup>1.5</sup>)

$Q/D^{2.5}$  = 2.44 ft<sup>0.5</sup>/s

Froude Number

Fr = 1.42

Tailwater/Adjusted Diameter **OR** Tailwater/Adjusted Rise

$Y_t/D$  = 0.51

Supercritical!

Inlet Control Headwater

$HW_i$  = 0.99 ft

Outlet Control Headwater

$HW_o$  = 0.64 ft

Design Headwater Elevation

HW = 5.641.31 ft

Headwater/Diameter **OR** Headwater/Rise Ratio

$HW/D$  = 0.99

Minimum Theoretical Riprap Size

$d_{50}$  = 2 in

Nominal Riprap Size

$d_{50}$  = 6 in

UDFCD Riprap Type

Type = VL

Length of Protection

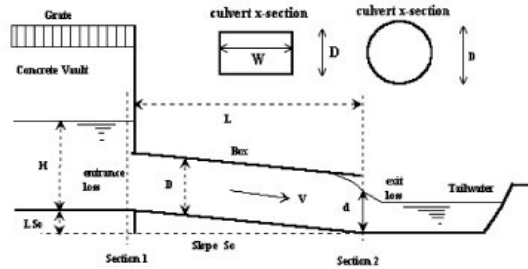
$L_p$  = 3 ft

Width of Protection

T = 2 ft

# CULVERT STAGE-DISCHARGE SIZING (INLET vs. OUTLET CONTROL WITH TAILWATER EFFECTS)

Project: **Eastern Hills South 4-65 17-18 3AH-3DH, 4AH-4DH Pad**  
 Basin ID: **Culvert D**  
 Status:



## Design Information (Input):

**Circular Culvert:** Barrel Diameter in Inches  
 Inlet Edge Type (choose from pull-down list)

D = 12 inches  
 Grooved End Projection

OR:

**Box Culvert:** Barrel Height (Rise) in Feet  
 Barrel Width (Span) in Feet  
 Inlet Edge Type (choose from pull-down list)

Height (Rise) = ft.  
 Width (Span) = ft.  
 Square Edge w/ 30-78 deg. Flared Wingwall

Number of Barrels  
 Inlet Elevation at Culvert Invert  
 Outlet Elevation at Culvert Invert OR Slope of Culvert (ft v./ft h.)  
 Culvert Length in Feet  
 Manning's Roughness  
 Bend Loss Coefficient  
 Exit Loss Coefficient

No = 1  
 Inlet Elev = 5640.32 ft. elev.  
 Slope = 0.013 ft vert. / ft horiz.  
 L = 45.5 ft.  
 n = 0.013  
 K<sub>b</sub> = 0  
 K<sub>x</sub> = 1

## Design Information (calculated):

Entrance Loss Coefficient  
 Friction Loss Coefficient  
 Sum of All Loss Coefficients  
 Orifice Inlet Condition Coefficient  
 Minimum Energy Condition Coefficient

K<sub>e</sub> = 0.20  
 K<sub>f</sub> = 1.42  
 K<sub>s</sub> = 2.62  
 C<sub>d</sub> = 0.95  
 KE<sub>low</sub> = -0.0898

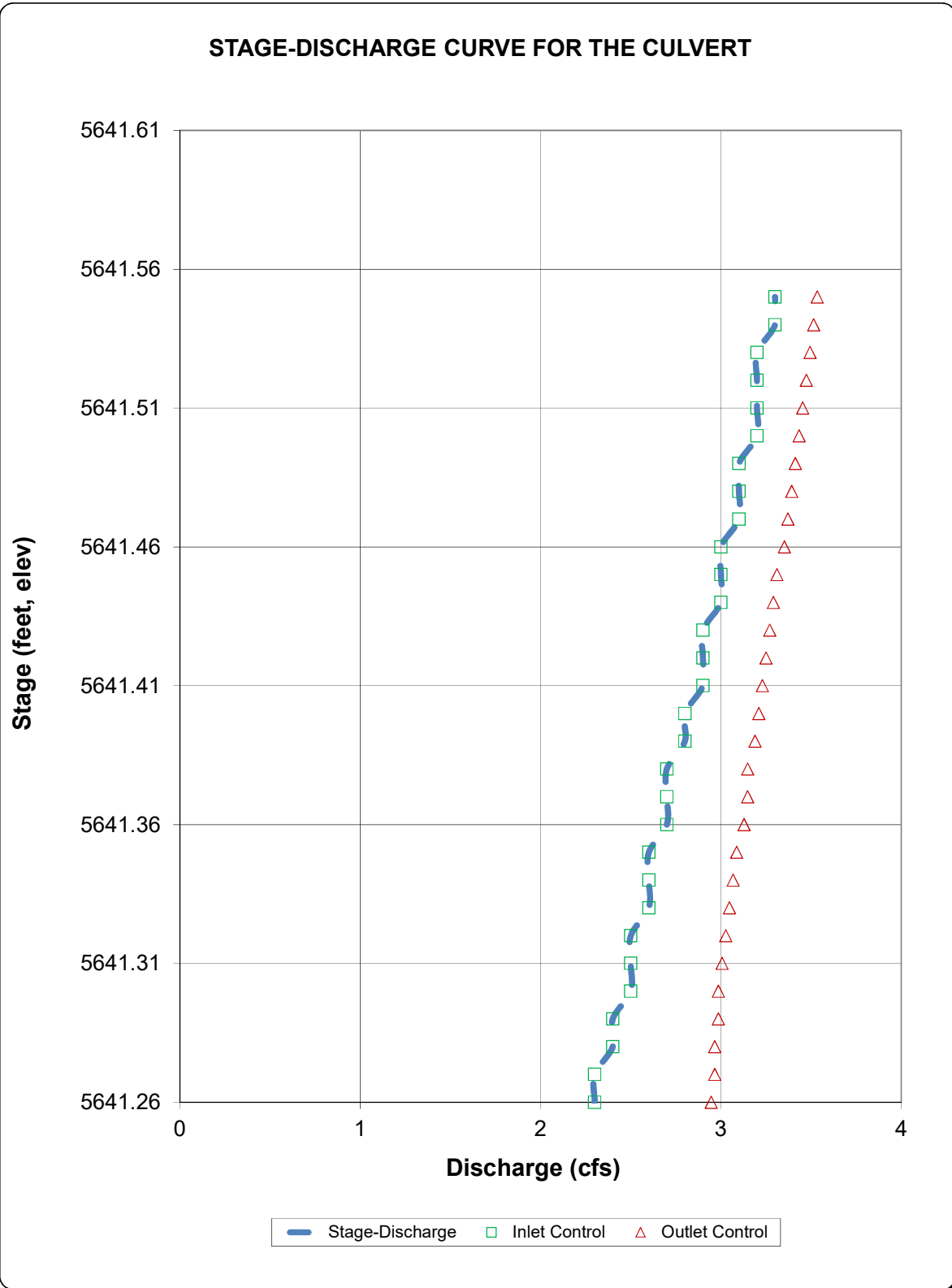
## Calculations of Culvert Capacity (output):

Water Surface Elevation (ft., linked)	Tailwater Surface Elevation ft	Culvert Inlet-Control Flowrate cfs	Culvert Outlet-Control Flowrate cfs	Controlling Culvert Flowrate cfs (output)	Inlet Equation Used:	Flow Control Used
5641.26		2.30	2.95	2.30	Regression Eqn.	INLET
5641.27		2.30	2.97	2.30	Regression Eqn.	INLET
5641.28		2.40	2.97	2.40	Regression Eqn.	INLET
5641.29		2.40	2.99	2.40	Regression Eqn.	INLET
5641.30		2.50	2.99	2.50	Regression Eqn.	INLET
5641.31		2.50	3.01	2.50	Regression Eqn.	INLET
5641.32		2.50	3.03	2.50	Regression Eqn.	INLET
5641.33		2.60	3.05	2.60	Regression Eqn.	INLET
5641.34		2.60	3.07	2.60	Regression Eqn.	INLET
5641.35		2.60	3.09	2.60	Regression Eqn.	INLET
5641.36		2.70	3.13	2.70	Regression Eqn.	INLET
5641.37		2.70	3.15	2.70	Regression Eqn.	INLET
5641.38		2.70	3.15	2.70	Regression Eqn.	INLET
5641.39		2.80	3.19	2.80	Regression Eqn.	INLET
5641.40		2.80	3.21	2.80	Regression Eqn.	INLET
5641.41		2.90	3.23	2.90	Regression Eqn.	INLET
5641.42		2.90	3.25	2.90	Regression Eqn.	INLET
5641.43		2.90	3.27	2.90	Regression Eqn.	INLET
5641.44		3.00	3.29	3.00	Regression Eqn.	INLET
5641.45		3.00	3.31	3.00	Regression Eqn.	INLET
5641.46		3.00	3.35	3.00	Regression Eqn.	INLET
5641.47		3.10	3.37	3.10	Regression Eqn.	INLET
5641.48		3.10	3.39	3.10	Regression Eqn.	INLET
5641.49		3.10	3.41	3.10	Regression Eqn.	INLET
5641.50		3.20	3.43	3.20	Regression Eqn.	INLET
5641.51		3.20	3.45	3.20	Regression Eqn.	INLET
5641.52		3.20	3.47	3.20	Regression Eqn.	INLET
5641.53		3.20	3.49	3.20	Regression Eqn.	INLET
5641.54		3.30	3.51	3.30	Regression Eqn.	INLET
5641.55		3.30	3.53	3.30	Regression Eqn.	INLET

Processing Time: 01.30 Seconds

## CULVERT STAGE-DISCHARGE SIZING (INLET vs. OUTLET CONTROL WITH TAILWATER EFFECTS)

Project: Eastern Hills South 4-65 17-18 3AH-3DH, 4AH-4DH Pad  
Basin ID: Culvert D





## Trapezoidal Sediment Basin Stage-Storage

### Worksheet

Project Name: Eastern Hills South 4-65 17-18 3AH-3DH, 4AH-4DH Pad

Location: Aurora, Colorado

#### Available Storage Calculation:

$$Volume = \frac{D}{3} (A_B + A_T + \sqrt{A_B A_T})$$

where:

D = incremental depth (ft)

A<sub>1</sub> = Bottom Area for increment (ft<sup>2</sup>)

A<sub>2</sub> = Top Area for increment (ft<sup>2</sup>)

Design Parameters:

Bottom Width:	78 ft
Bottom Length:	156 ft
Bottom Elevation:	5637.00

Elevation	Surface Area	(1/3)*A + B + (A*B)^0.5	Incremental Depth	Incremental Volume	Cumulative Volume
	(square feet)		(feet)	(cubic feet)	(cubic feet)
5637.00	12168	0.00	0.00	0.00	-
5637.25	12521	12344.08	0.25	3086.02	3,086.0
5637.50	12879	12699.58	0.25	3174.89	6,260.9
5638.00	13608	13241.83	0.50	6620.91	12,881.8
5638.50	14355	13979.84	0.50	6989.92	19,871.7

Available Storage at Spillway: 19,872 cf

#### Required Storage Calculation:

Disturbance Area (11.45 ac.) - Reclaimed Pad (4.42 ac.) = 7.03 ac.

This 7.03 acre tributary area is comprised of approximately 6.48 acres of reclaimed grass and seeded stockpiles (10% impervious) in addition to the approximately 0.55 acre sediment basin (90% impervious).

Table 1 of the COA Storm Drainage Design and Technical Criteria Manual was used to determine the percent impervious estimates.

Using UDFCD Table SB-1: (6.48 ac. X 800 cf/ac.) + (0.55 ac. X 5,300 cf/ac.) = 8,099 cf

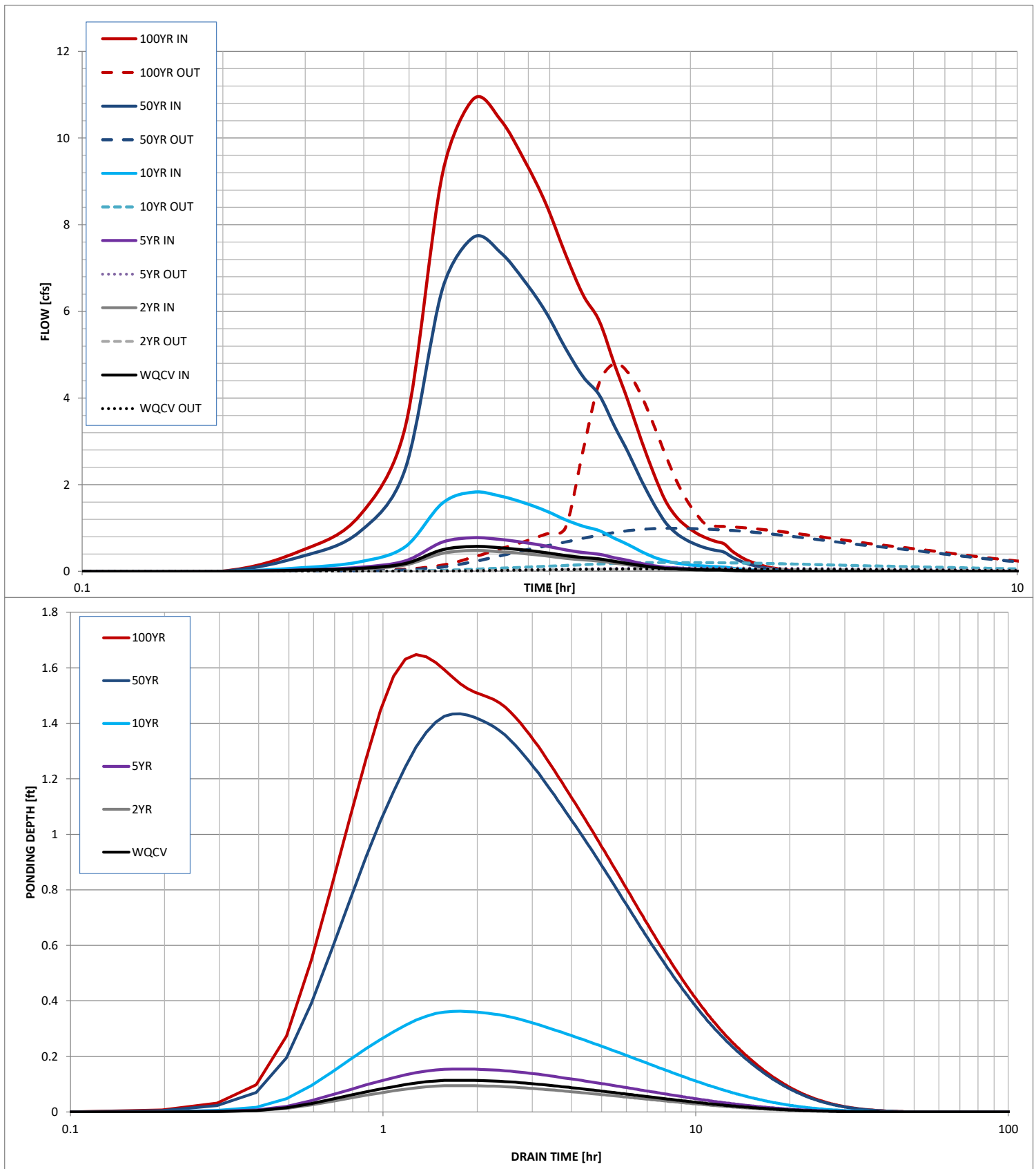
Required Storage Volume:	8,099 cf
--------------------------	----------

POND ADEQUATELY SIZED

Worksheet Protected

**Facility Location & Jurisdiction:** Section 17, T4S, R65W, City of Aurora, Arapahoe County, Colorado

## Stormwater Detention and Infiltration Design Data Sheet



STAGE-DISCHARGE SIZING OF THE WATER QUALITY CAPTURE VOLUME (WQCV) OUTLET	
--	--

Project: **Eastern Hills South 4-65 17-18 3AH-3DH, 4AH-4DH Pad**

Basin ID: **Orifice Holes**

**WQCV Design Volume (Input):**

5637.256

**Watershed Design Information (Input):**

Perforated Plate Examples

4"

**Outlet Design Information (Output):**

[illegible]

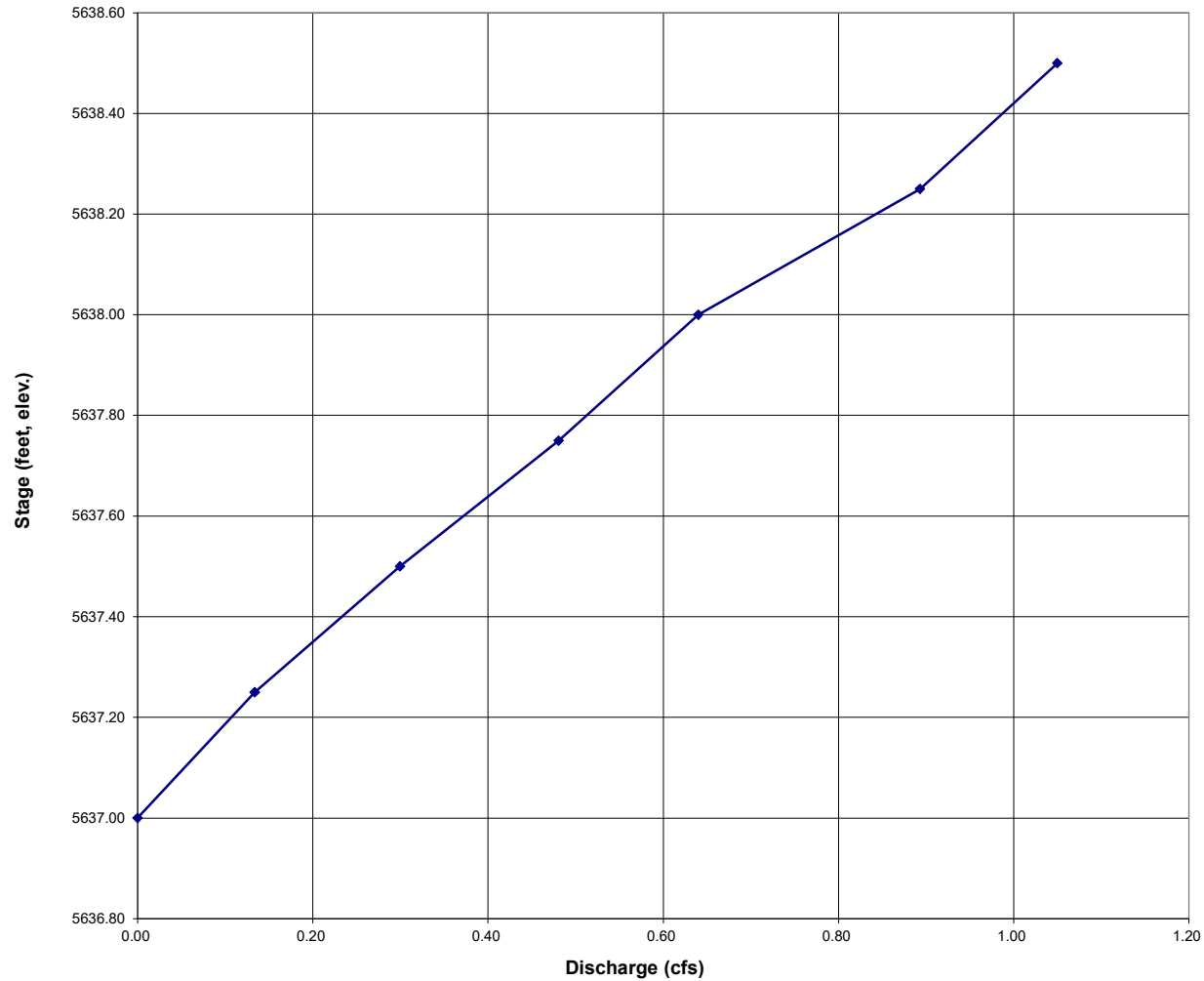
## STAGE-DISCHARGE SIZING OF THE WATER QUALITY CAPTURE VOLUME (WQCV) OUTLET

Worksheet Protected

Project: Eastern Hills South 4-65 17-18 3AH-3DH, 4AH-4DH Pad

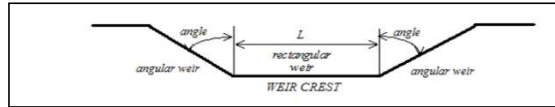
Basin ID: Orifice Holes

STAGE-DISCHARGE CURVE FOR THE WQCV OUTLET STRUCTURE



## STAGE-DISCHARGE SIZING OF THE SPILLWAY

**Basin ID:** Sediment Basin - Spillway



**Design Information (input):**

L =	11.00	feet
Angle =	75.96	degrees
EL. Crest =	5,638.50	feet
C <sub>w</sub> =	3.00	
C <sub>t</sub> =	3.00	

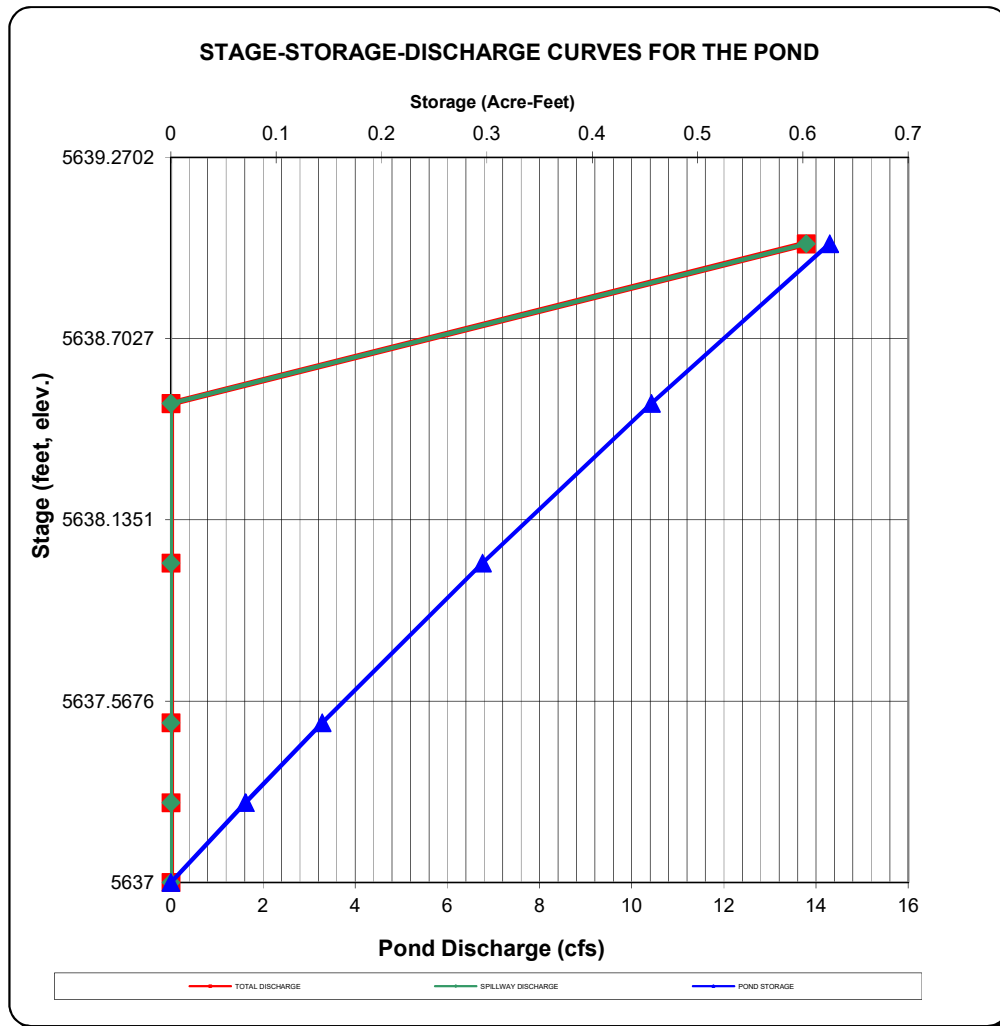
**Calculation of Spillway Capacity (output):**

[illegible]

## STAGE-DISCHARGE SIZING OF THE SPILLWAY

Project: Eastern Hills South 4-65 17-18 3AH-3DH, 4AH-4DH Pad

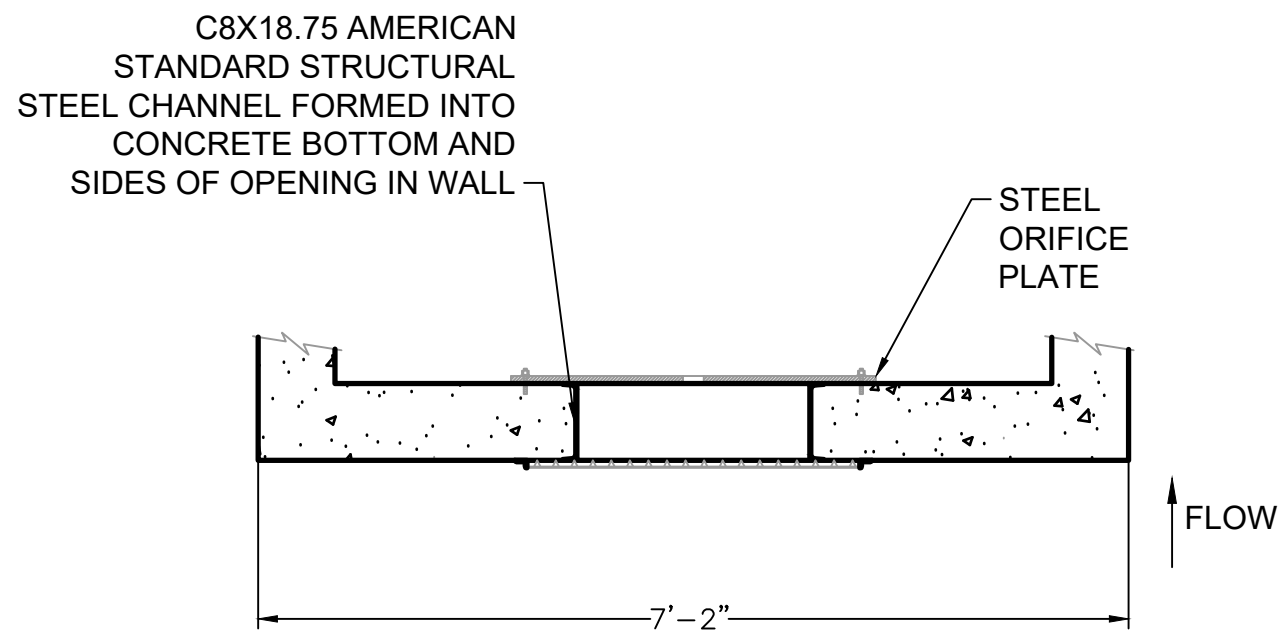
Basin ID: Sediment Basin - Spillway



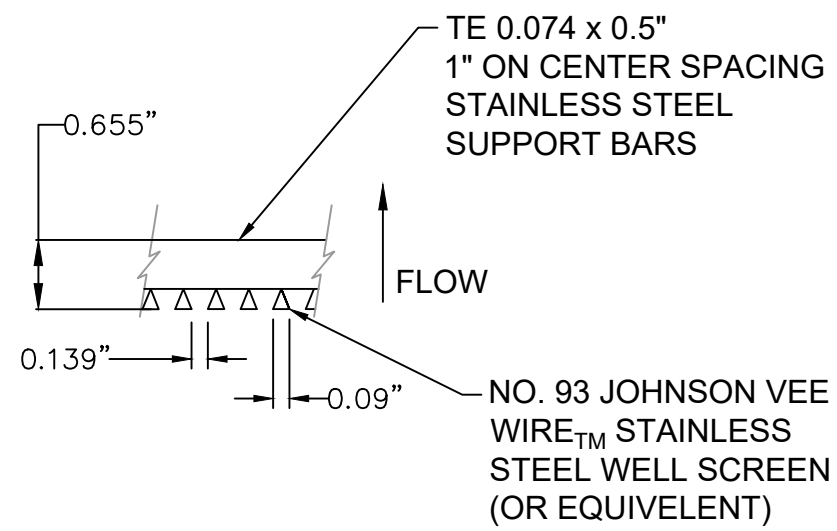
EASTERN HILLS SOUTH 4-65 17-18 3AH-3DH, 4AH-4DH PAD

OUTLET STRUCTURE TABLE						
POND ID	BOX TOP ELEVATION	WSE ①	MICROPOOL WSE ②	OUTLET PIPE INVERT ELEVATION ③	BOX BOTTOM ELEVATION ④	BOX HEIGHT FRONT (H) ft.
EASTERN HILLS	5638.50	5638.50	5637.00	5636.75	5633.50	5.00

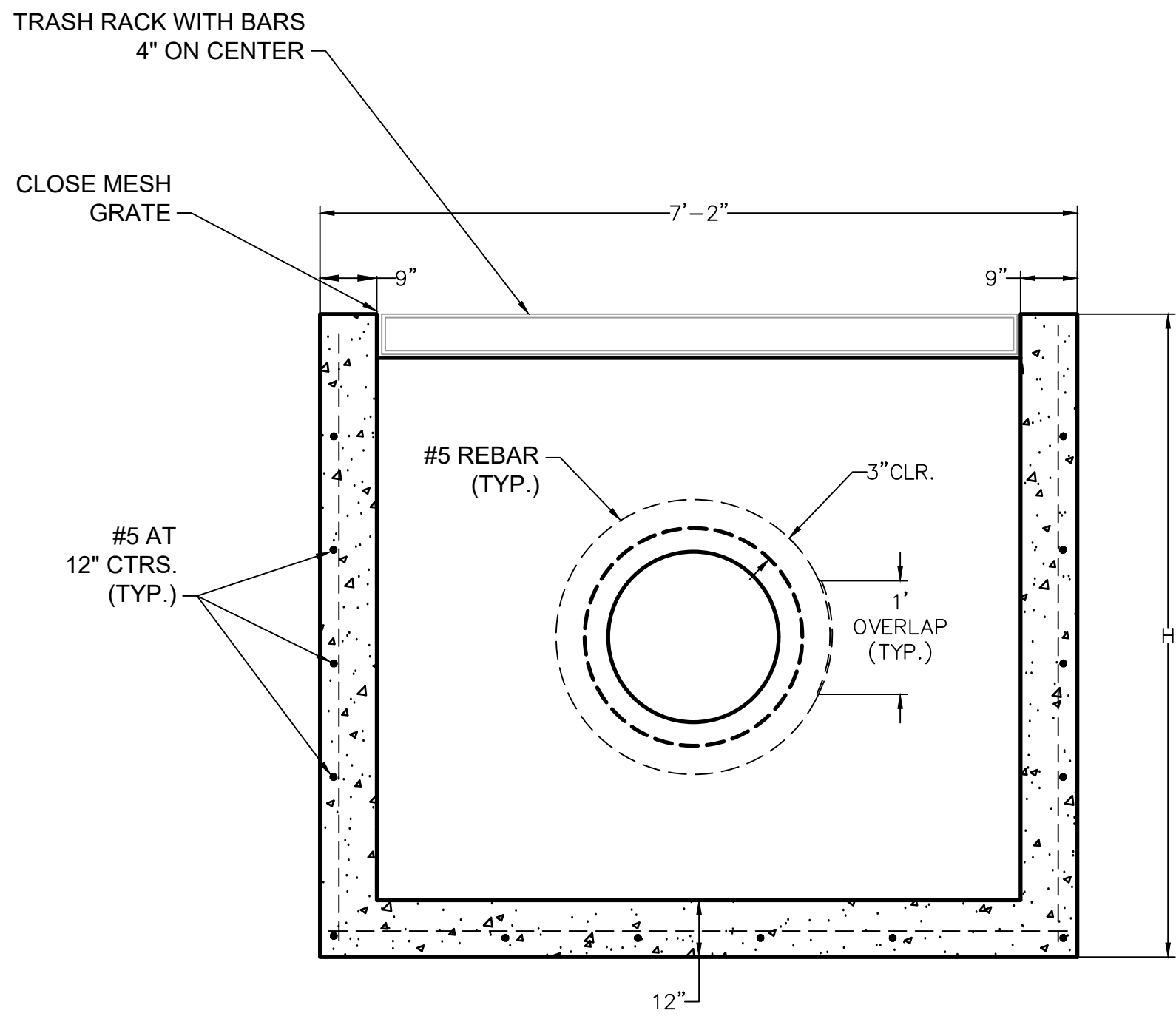
CONCRETE OPENING AND ORIFICE PLATE DETAIL TABLE									
POND ID	CONCRETE OPENING TOP ELEVATION ⑤	CONCRETE OPENING BOTTOM ELEVATION ⑥	CONCRETE OPENING HEIGHT (HO) ft.	CONCRETE OPENING WIDTH (WO) ft.	ORIFICE PLATE TOP ⑦	ORIFICE PLATE BOTTOM ⑧	BOTTOM HOLE ELEVATION ⑨	# OF ROWS	# OF COLUMNS
EASTERN HILLS	5638.50	5634.82	3.68	2.00	5638.50	5634.57	5637.00	4	1



SECTION D  
NTS

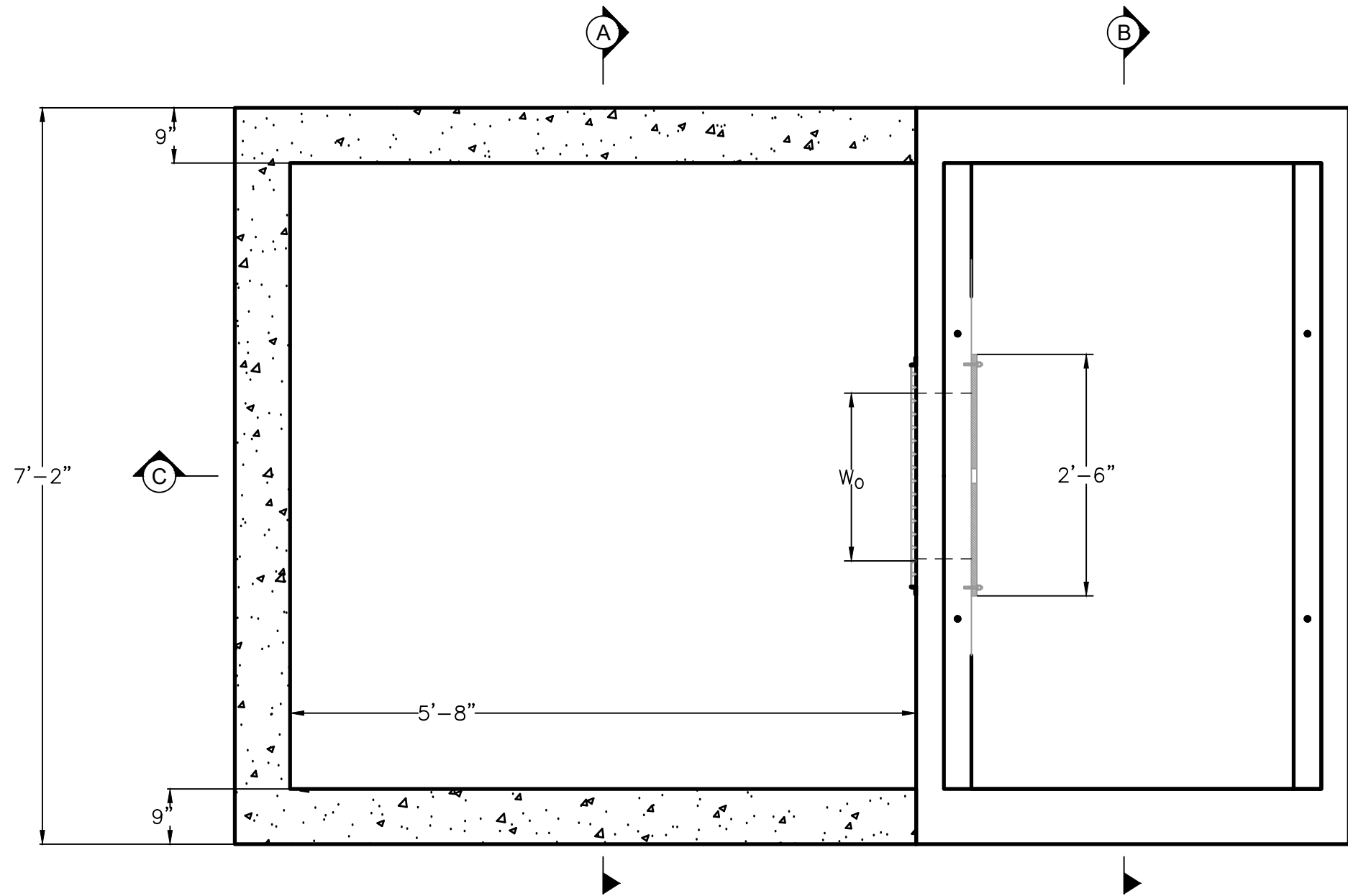


SECTION E  
NTS

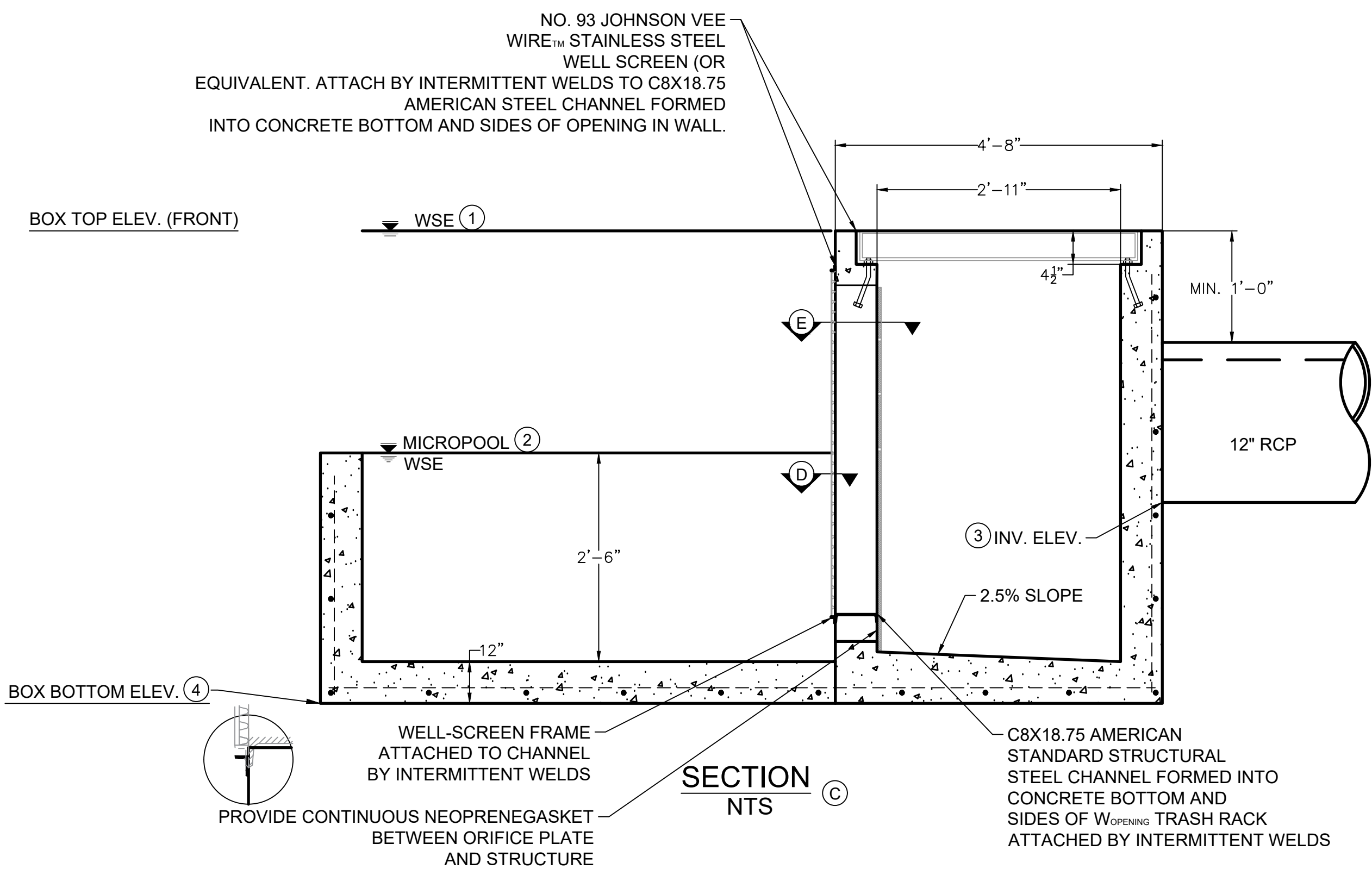


SECTION B  
NTS

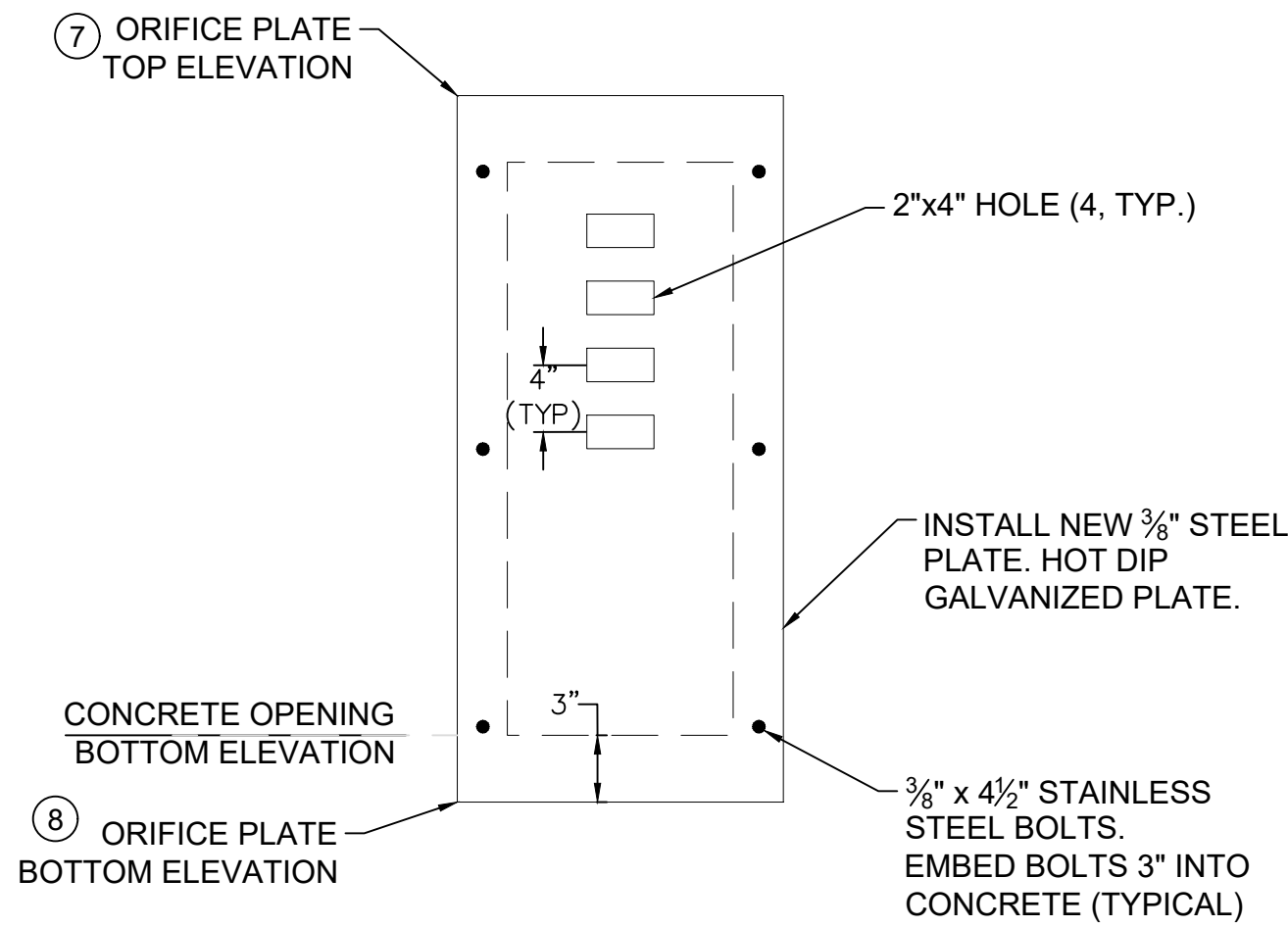
NOTE: REFER TO CDOT TYPE D INLET(M-604-11) FOR REINFORCING BAR SIZE & SPACING.



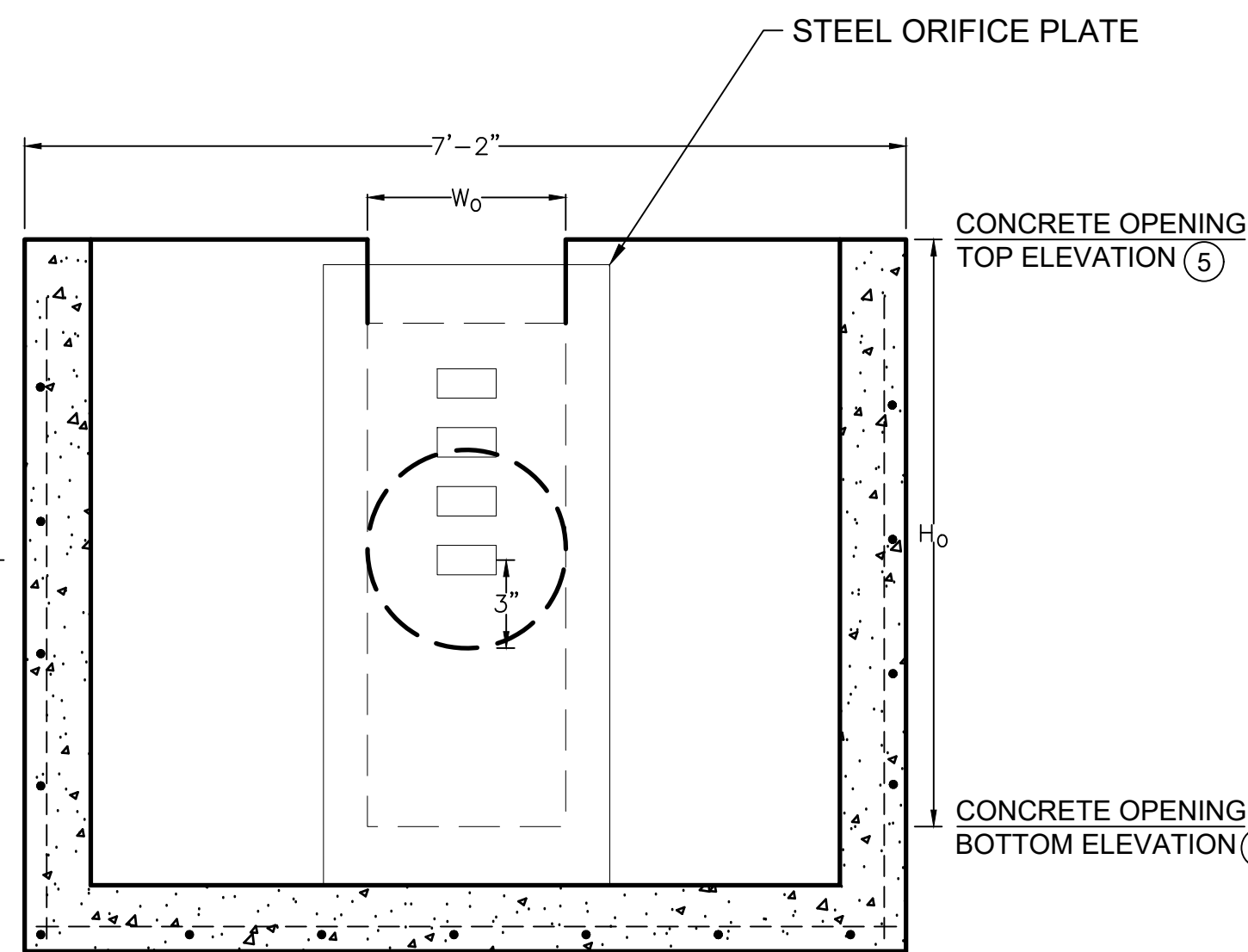
PLAN VIEW  
(SHOWING ANCHOR BOLT LAYOUT)



SECTION C  
NTS



ORIFICE PLATE DETAIL  
NTS



SECTION A  
NTS

NOTE: SHOWN WITHOUT TRASH SCREEN

PREPARED BY:



Ascent Geomatics Solutions  
8620 Wolff Court  
Westminster, CO 80031

PREPARED FOR:



CONOCOPHILLIPS COMPANY  
34501 E. QUINCY AVE., BLDG. 1  
WATKINS, CO 80137

SHEET NAME:  
OUTLET STRUCTURE DETAILS  
SURFACE LOCATION:  
E 1/2 SE 1/4 SECTION 17, TOWNSHIP 4 SOUTH,  
RANGE 65 WEST, 8TH RANGE  
ARAPAHO COUNTY, COLORADO

INT.

LM

REVISION DESCRIPTION

ISSUED FOR REVIEW

DATE:

01/27/20

NO.

0

FIELD DATE:

02-15-2018

DRAWING DATE:

01-24-2020

DRAFTED BY:

LM

SHEET NO.

D1